

DRAINAGE REPORT

FOR

ROQUET RANCH – TTM 19983 CITY OF COLTON

Prepared for:

SUNMEADOWS, LLC
27127 Calle Arroyo, Suite 1910
San Juan Capistrano, CA 92675

Prepared by:



Engineering, Inc.

357 N. Sheridan Street, Suite 117
Corona, CA 92880
Phone: (951) 279-1800
Fax: (951) 279-4380

JN: 269.335 / 316.452



February 2016

TABLE OF CONTENTS

Section	Page
INTRODUCTION.....	3
EXISTING CONDITIONS.....	5
PROPOSED CONDITIONS	6
METHODOLOGY.....	8
HYDROLOGY RESULTS	8
HYDRAULICS.....	21
CONCLUSIONS.....	27
REFERENCES.....	28

FIGURES

1a	Location Map
1b	Aerial Pictures
1c	Land Use Map
2	Hydrology Map – Existing Condition
3	Hydrology Map – Proposed Condition

ATTACHMENTS

- **A:** Rational Method Calculations:
 - Existing Condition: 10-yr and 100-yr storm
- **B:** Rational Method Calculations, main line storm drain:
 - Proposed Condition: 10-yr and 100-yr storm

INTRODUCTION

PURPOSE

This drainage study has been prepared in order to support the drainage system design of the Roquet Ranch – TTM 19983 development. This report identifies drainage patterns and offsite flow tributary to this subject site and provides evaluation runoff from the site under full development as Mix Use Development. The primary purpose of the calculations is to design storm drain system within the project and to provide hydraulic calculations for the proposed Roquet Ranch Storm Drain systems.

Roquet Ranch project comprises approximately 335 acres and is a mixed use development which will include a school site, commercial area, apartments, various open spaces and a public park. Residential development will be the primary development with 900 dwelling units proposed. Project located at La Loma Hills, west of La Cadena Drive, east of Santa Ana River and north of County of Riverside boundary in City of Colton. The project bounded on the south by residential development and the Riverside/San Bernardino County Line, on the west by the Santa Ana River, on the north by vacant land, and on the east by residential developments and La Cadena Drive.

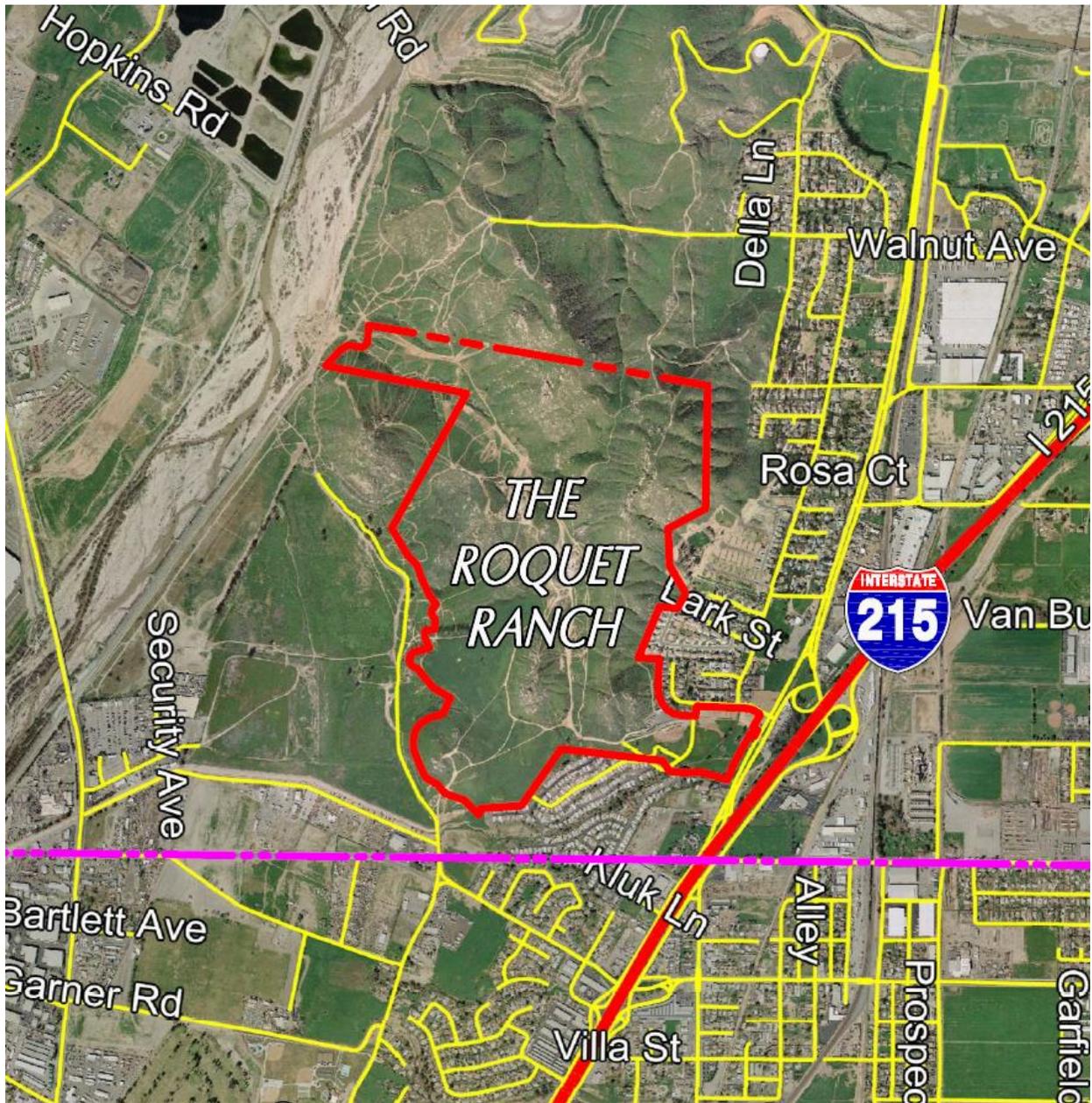
SETTING

The project study is located at La Loma Hills, west of La Cadena Drive, east of Santa Ana River and north of County of Riverside boundary in City of Colton, in southerly San Bernardino County. Most of the immediate surrounding areas are either developed or planned for the development of single family residential neighborhoods and commercial uses, or comprise undeveloped vacant land.

See Figure 1a - Vicinity Map.

The site ranges in elevation from approximately 850 feet above mean sea level in the southwest corner of the site to approximately 1480 feet above mean sea level.

With the City of Colton being a co-permitee on San Bernardino Counties' MS4 permit, certain post development water quality features need to be designed into the project for water quality treatment of daily nuisance flows and first flush storm flows after the project is constructed and homes are occupied.



Roquet Ranch

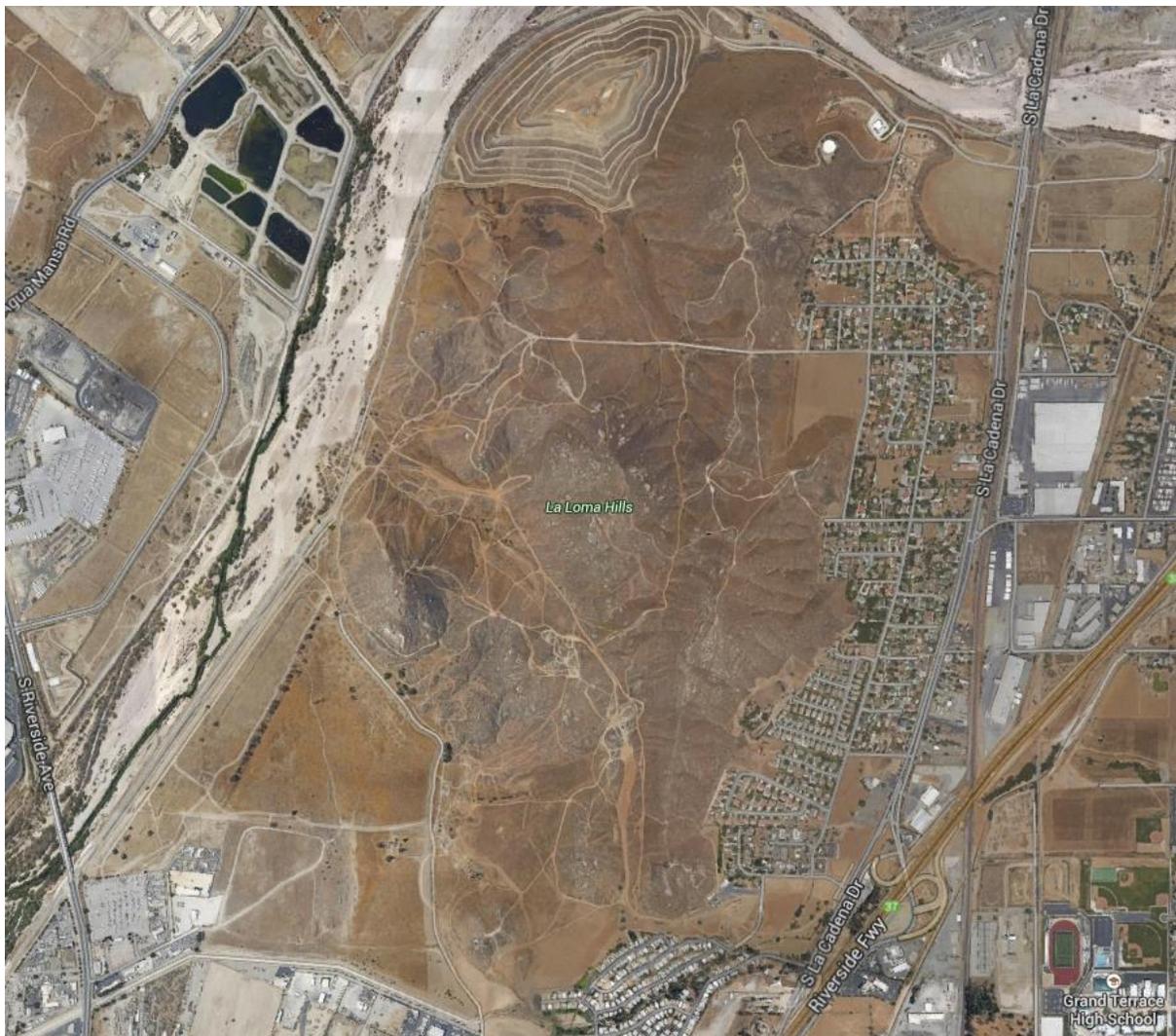
Figure 1a: Vicinity Map

EXISTING CONDITIONS

The Roquet Ranch – TTM 19983 projects comprises approximately 335 acres and is located at La Loma Hills, west of La Cadena Drive, east of Santa Ana River and north of County of Riverside boundary in City of Colton, California. The majority of the site is currently vacant with an overhead electric power transmission line that generally bisects the property, trending southeast in the northern portion of the property and north-south in the central portion of the site. Along the southern boundary of the site, the transmission line turns to the east and exits the site at the eastern boundary.

Numerous dirt access roads and trails cross the site. Numerous dirt access roads and trails cross the site. There are a few piles of stockpiled material as well as debris and trash in the central portion of the site. Various equipment and stockpiles of asphalt grindings associated with Roquet Paving operations were observed in the southeastern portion of the site.

Plant growth currently consists of an assortment of native grasses and brush, with very heavy vegetation in some areas, as well as a few mature trees occurring in the southwestern portion of the site. The steeper hillside areas of the site have little to no vegetation due to the rock outcrops. Some of the gently sloping low lying areas appear to have been recently disked.



**Figure 1b: Aerial Picture
Current Condition**

Hydrology - Existing Condition:

Hydrologic parameters used in this analysis are as presented in the San Bernardino County Hydrology Manual.

There are two (2) watersheds drainage areas in this study, Drainage Area A drains to Highgrove Channel along the southern boundary of the project side. Drainage Area B drains to northwest toward Santa Ana River.

The first watershed Drainage Area A is approximately 184 acres, consists of several streams (sub-drainage areas AA through AI) tributary to the majority of the project site except the northern portion. Drainage Area A is tributary to existing Highgrove Channel along the south side of the project boundary.

The second watershed Drainage Area B is approximately 157 acres, tributary to the northern portion of the project site. Drainage Area B is tributary to Santa Ana River.

PROPOSED CONDITIONS

Roquet Ranch is a mixed use development which will include mixed density residential, neighborhood commercial, public institution, various open spaces and a public park. Residential development will be the primary development with approximately 900 dwelling units proposed.

The proposed street alignments and rough grading as shown on the Hydrology Maps were used to modify the natural drainage patterns and boundaries to determine the post-development hydrology.

Drainage patterns will generally remain as in the existing condition as much as practical.

Hydrology - Proposed Condition:

Hydrologic parameters used in this analysis are as presented in the San Bernardino County Hydrology Manual.

There are two (2) watersheds drainage areas in this study, Drainage Area A drains to Highgrove Channel along the southern boundary of the project side. Drainage Area B drains to northwest toward Santa Ana River.

The first watershed Drainage Area A (drainage subareas AA through AH) is approximately 188 acres from the project site and tributary to the existing Highgrove Channel.

The second watershed Drainage Area B is approximately 100 acres and tributary direct to the Santa Ana River.

See Land Use Map below for project proposed land use used in the proposed condition hydrology calculation.

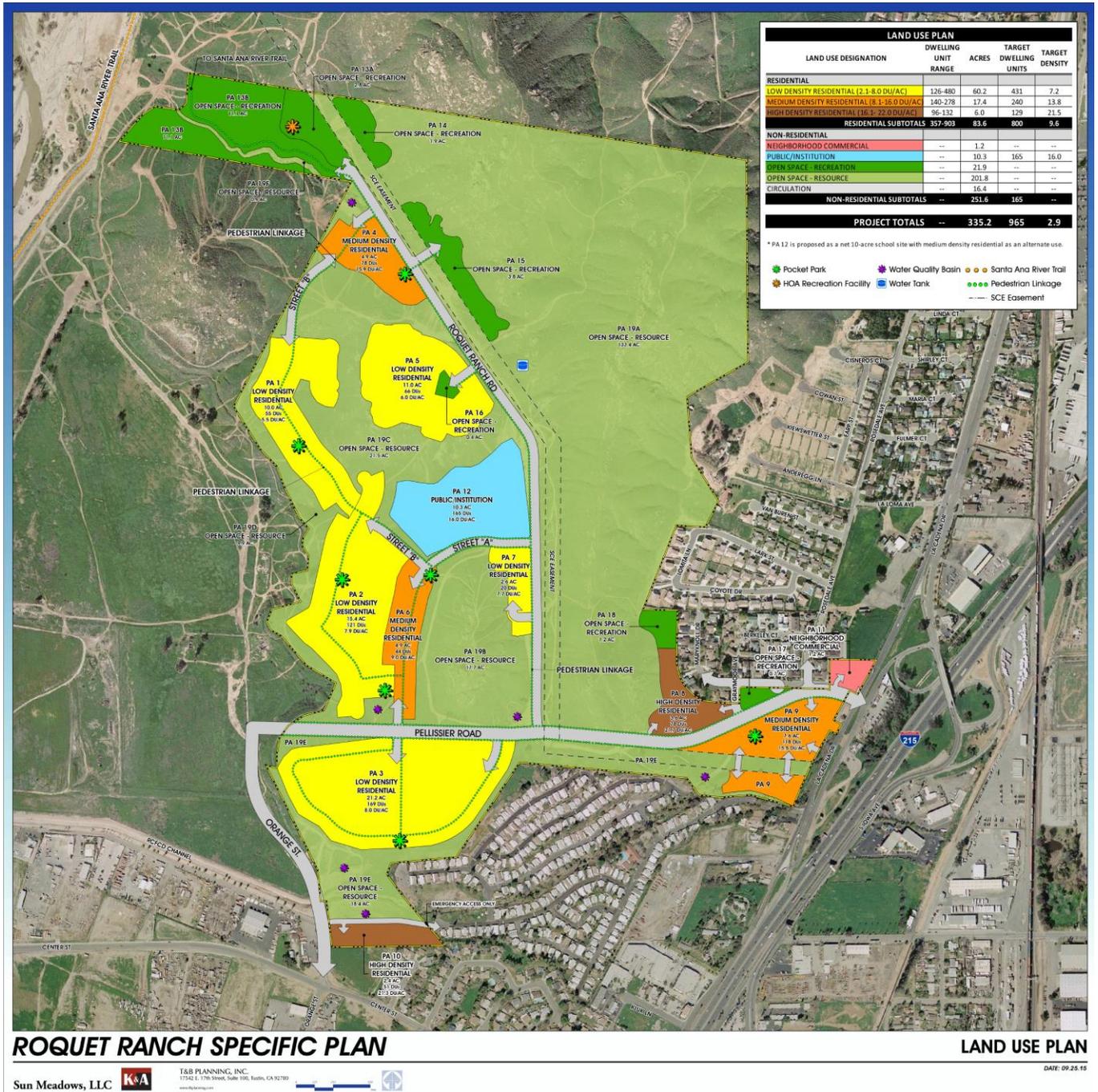


Figure 1c: Land Use Map

METHODOLOGY

The hydrology calculations for determining the on-site and offsite flows have been conducted using the Rational Method as incorporated into the CivilCADD Rational Method Hydrology software. The rational method relates rainfall intensity, the ratio of runoff to rainfall, and the drainage area size to the peak storm runoff and is expressed by the equation: $Q = CIA$. Where Q = runoff (in cubic feet per second), C = runoff coefficient relating the ratio of runoff to rainfall, I = rainfall intensity (in inches per hour), A = drainage area (in acres).

The San Bernardino County uses the SCS soils classification system, which classifies soils into four (4) types: A through D with D being the least pervious, thus providing the highest runoff potential.

The soil type used in the analysis is a majority Type C. Applicable soil types and limits are shown on the enclosed hydrology maps.

Figure 2 and Figure 3 are the onsite, off-site existing and proposed condition hydrology maps, respectively, summarize the results of the hydrologic analysis, including drainage areas, subareas, node numbers, elevations and cumulative Q_{10} and Q_{100} values at points of concentration or discharge.

RESULTS

The design discharge in the various sub-drainage areas considered in this study are listed in the table below:

Summary Hydrology Drainage Sub-areas for Existing Condition – Rational Method 10-year storm (see Attachment for calculation):

Drainage Area	Area in Acre	Q_{10} sub-area in cfs	Q_{10} conf. in cfs
AA-1	7.85	15.65	
AA-2	5.15	7.72	23.37
AB-1	5.73	11.42	
AB-2	9.85	15.68	27.09
AC-1	4.85	9.67	
AC-2	9.49	14.94	24.61
AC-3	16.54	23.48	48.09
AC-4	20.50	21.18	69.27
AD-1	3.73	5.81	
AE-1	7.05	12.11	
AE-2	20.10	32.83	44.94
AF-1	4.17	7.92	
AF-2	14.92	22.86	30.78
AG-1	7.10	12.58	
AG-2	10.12	15.03	27.62

AG-3	14.64	17.78	45.40
AH-1	8.12	15.11	
AI-1	8.64	14.04	
AI-2	11.54	18.75	32.79
BA-1	6.99	13.17	
BA-2	8.23	12.88	26.05
BA-3	19.54	27.78	53.83
BA-4	35.41	44.62	98.45
BA-5	87.05	98.77	197.22

Summary Hydrology Drainage Sub-areas for Existing Condition – Rational Method 100-year storm (see Attachment for calculation):

Drainage Area	Area in Acre	Q ₁₀₀ sub-area in cfs	Q ₁₀₀ conf. in cfs
AA-1	7.85	23.27	
AA-2	5.15	12.04	35.31
AB-1	5.73	16.98	
AB-2	9.85	24.14	41.12
AC-1	4.85	14.37	
AC-2	9.49	23.17	37.55
AC-3	16.54	36.87	74.42
AC-4	20.50	35.21	109.62
AD-1	3.73	8.75	
AE-1	7.05	18.16	
AE-2	20.10	49.61	67.77
AF-1	4.17	11.80	
AF-2	14.92	35.31	47.11
AG-1	7.10	18.82	
AG-2	10.12	23.19	42.01
AG-3	14.64	28.33	70.34
AH-1	8.12	22.55	
AI-1	8.64	21.11	
AI-2	11.54	28.20	49.31
BA-1	6.99	19.64	
BA-2	8.23	19.83	39.46
BA-3	19.54	43.32	82.64
BA-4	35.41	70.85	153.64
BA-5	87.05	159.27	312.91

Summary Hydrology Drainage Sub-areas for Proposed Condition – Rational Method
 10-year storm (see Attachment for calculation):

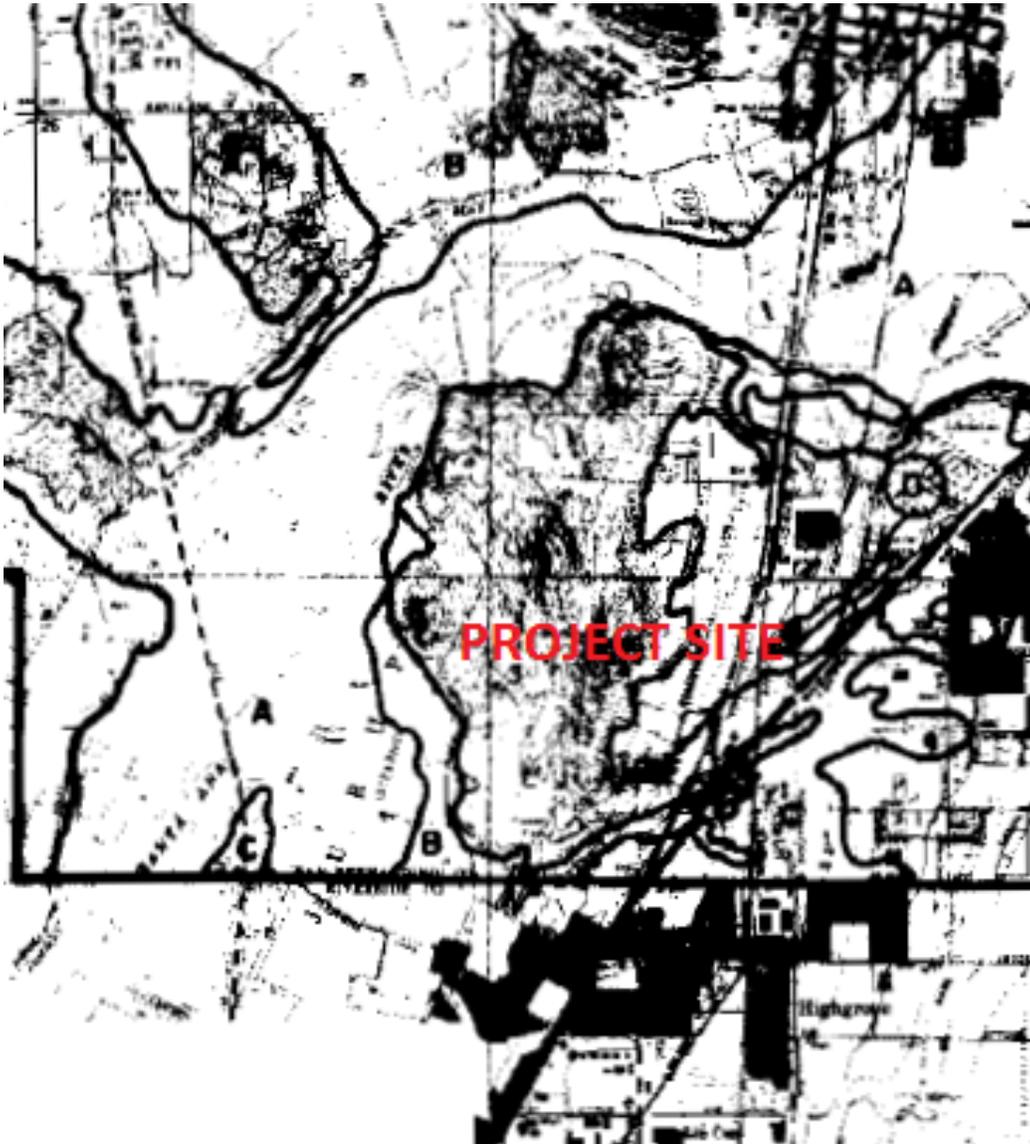
Drainage Area	Area in Acre	Q ₁₀ sub-area in cfs	Q ₁₀ conf. in cfs
AA-1	5.70	10.90	
AA-2	6.46	10.17	21.07
AA-3	5.40	6.97	28.04
AA-4	4.28	6.90	34.95
AA-5	3.84	4.80	39.75
AA-6	1.08	1.27	41.02
AA-7	4.47	8.41	
AA-8	4.28	6.86	15.27
AA-9	1.15	3.56	
AA-10	1.75	3.54	7.09
		Node 105	59.24
AA-11	7.60	13.68	
		Node 111	72.61
AA-12	4.46	7.80	
AA-13	6.96	12.52	20.32
AA-14	1.59	3.10	23.41
AA-15	7.23	8.82	32.24
AA-16	2.64	3.05	35.29
AA-17	3.57	5.41	40.70
		Node 120	110.99
AB-1	4.88	8.64	
AB-2	6.02	9.48	18.12
AB-3	10.20	16.96	35.08
AB-4	2.35	2.61	37.68
AC-1	3.13	7.65	
AC-2	3.75	5.24	12.89
AC-3	0.46	0.73	13.62
AD-1	2.24	4.91	
AE-1	5.25	11.05	
AE-2	11.80	22.02	33.06
AE-3	3.85	5.51	38.57
AE-4	5.88	8.82	47.38
AE-5	3.86	2.54	49.92
AE-6	3.85	6.27	56.20
AF-1	4.38	11.64	
AF-2	4.54	12.06	23.70
AF-3	10.20	25.48	49.18
AF-4	1.29	2.77	51.95
BA-1	5.14	10.29	
BA-2	5.32	9.47	19.76

	1.00	2.08	21.84
BA-3	25.60	48.37	70.21
BA-4	17.80	30.19	100.39
BA-5	2.53	4.14	104.53
	1.00	2.01	106.54
BA-6	2.41	6.08	
BA-7	9.05	19.86	25.94
BA-8	0.77	1.33	27.27
		NODE 704	130.69
BA-9	18.70	23.47	154.17
BA-10	8.80	14.98	
	2.00	3.78	172.93
		NODE 705	172.93
AG-1	5.27	10.83	
AH-1	4.10	9.00	
AH-2	5.85	12.84	21.84
AH-3	12.41	27.37	49.21

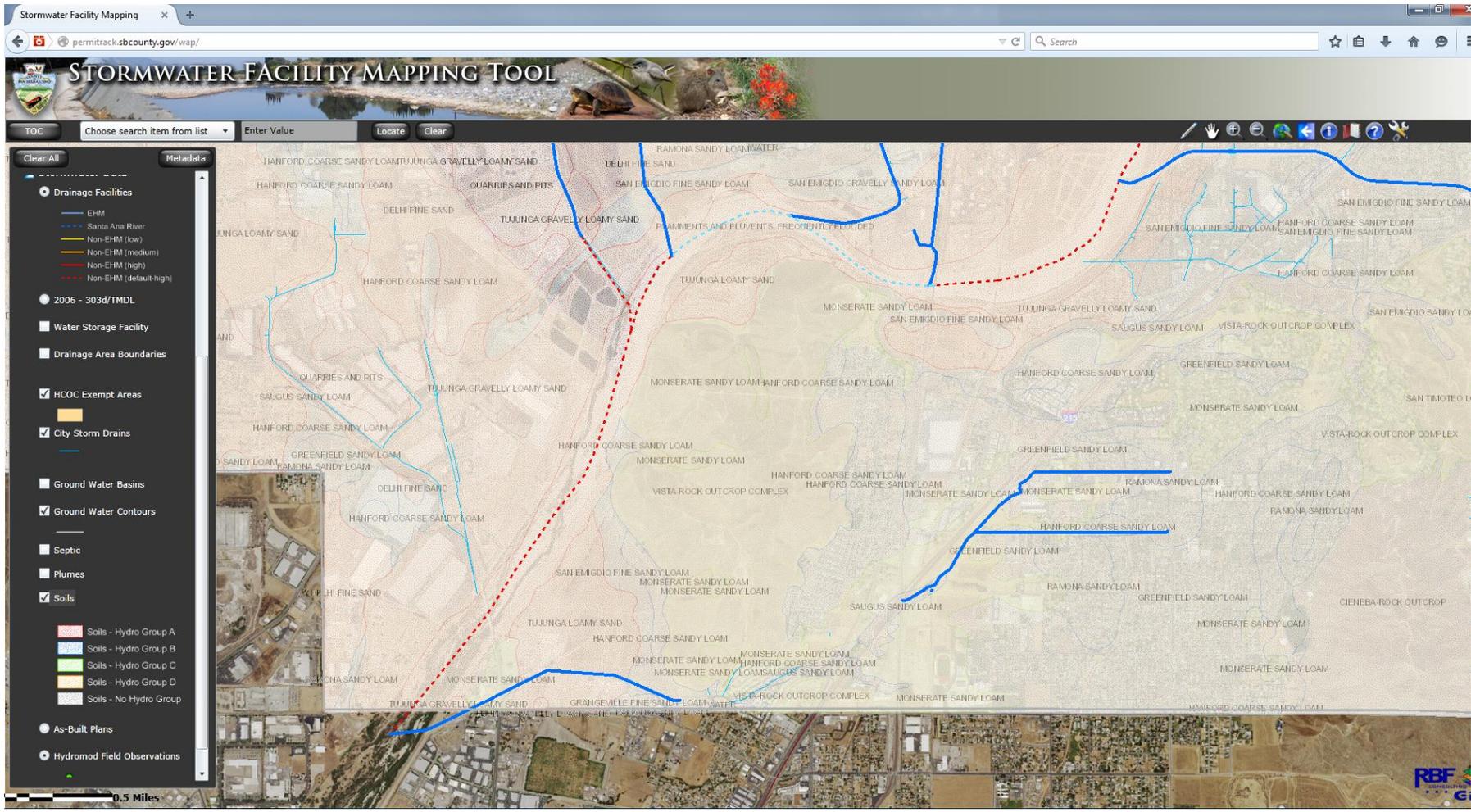
Summary Hydrology Drainage Sub-areas for Proposed Condition – Rational Method
100-year storm (see Attachment for calculation):

Drainage Area	Area in Acre	Q ₁₀₀ sub-area in cfs	Q ₁₀₀ conf. in cfs
AA-1	5.70	15.96	
AA-2	6.46	15.18	31.14
AA-3	5.40	10.63	41.77
AA-4	4.28	10.25	52.02
AA-5	3.84	7.32	59.34
AA-6	1.08	2.03	61.37
AA-7	4.47	12.32	
AA-8	4.28	10.24	22.56
AA-9	1.15	5.04	
AA-10	1.75	5.19	10.23
		Node 105	88.39
AA-11	7.60	20.05	
		Node 111	105.73
AA-12	4.46	11.47	
AA-13	6.96	18.24	29.70
AA-14	1.59	4.40	34.11
AA-15	7.23	13.62	47.72
AA-16	2.64	4.69	52.41
AA-17	3.57	8.08	60.50
		Node 120	166.15
AB-1	4.88	12.39	
AB-2	6.02	13.78	26.17
AB-3	10.20	24.49	50.65
AB-4	2.35	4.04	54.69
AC-1	3.13	10.86	
AC-2	3.75	7.81	18.67
AC-3	0.46	1.10	19.78
AD-1	2.24	7.03	
AE-1	5.25	16.11	
AE-2	11.80	32.61	48.72
AE-3	3.85	8.44	57.16
AE-4	5.88	13.42	70.57
AE-5	3.86	4.48	75.05
AE-6	3.85	9.43	84.48
AF-1	4.38	16.52	
AF-2	4.54	17.12	33.64
AF-3	10.20	36.51	70.16
AF-4	1.29	4.08	74.24
BA-1	5.14	15.03	
BA-2	5.32	14.06	29.10
	1.00	2.97	32.07

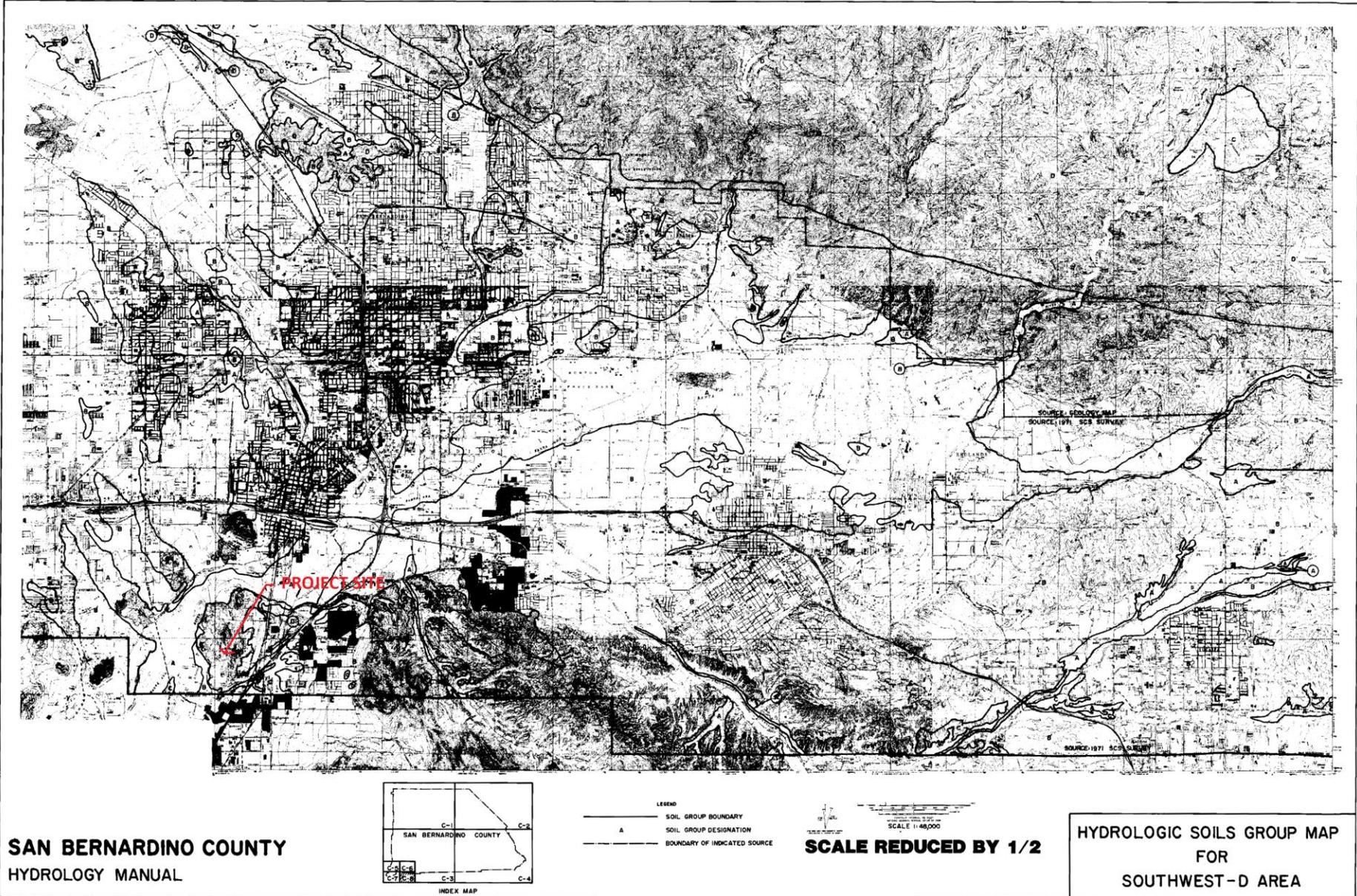
BA-3	25.60	71.21	103.27
BA-4	17.80	45.03	148.30
BA-5	2.53	6.19	154.50
	1.00	2.88	157.37
BA-6	2.41	8.63	
BA-7	9.05	28.77	37.40
BA-8	0.77	2.01	39.41
		NODE 704	192.24
BA-9	18.70	36.62	228.86
BA-10	8.80	22.34	251.20
	2.00	5.46	
		NODE 705	256.66
AG-1	5.27	15.81	
AH-1	4.10	13.11	
AH-2	5.85	18.71	31.82
AH-3	12.41	39.13	70.95



HYDROLOGIC SOILS GROUP

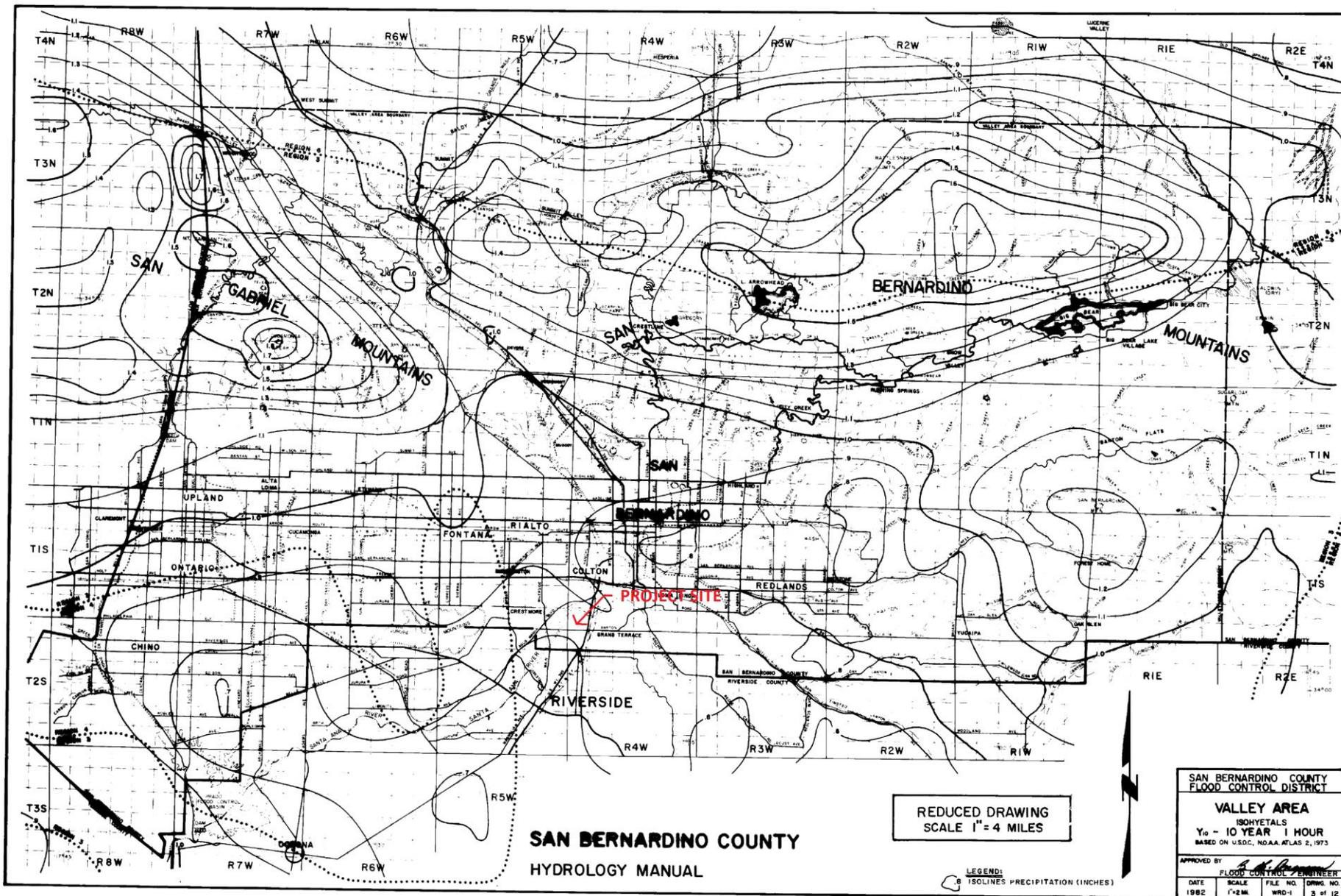


GIS Soil Map



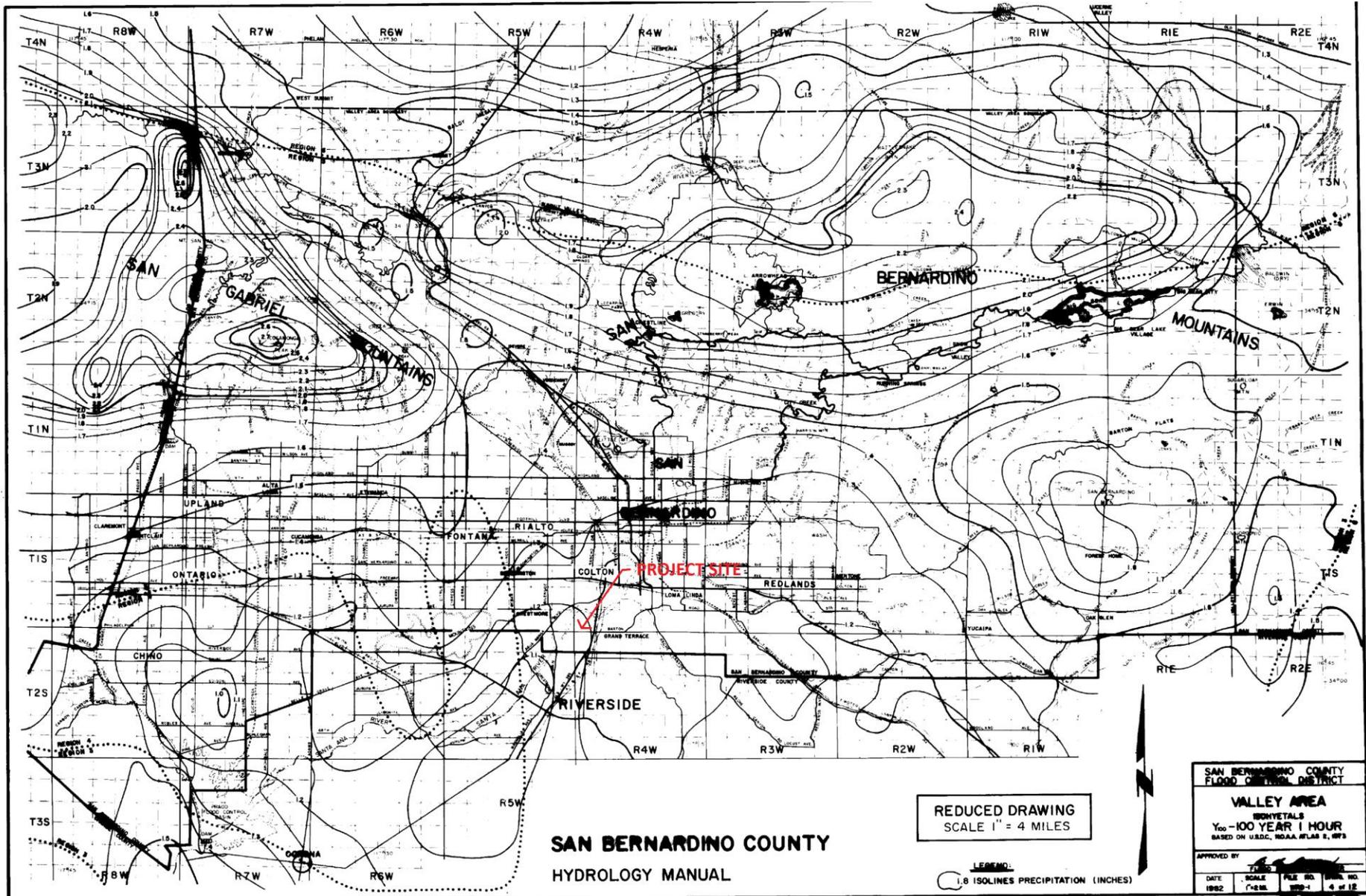
C-29

FIGURE C-16



B-11

FIGURE B-3



B-12

FIGURE B-4

Curve (I) Numbers of Hydrologic Soil-Cover Complexes For Pervious Areas-AMC II					
Cover Type (3)	Quality of Cover (2)	Soil Group			
		A	B	C	D
<u>NATURAL COVERS -</u>					
Barren (Rockland, eroded and graded land)		78	86	91	93
Chaparral, Broadleaf (Manzonita, ceanothus and scrub oak)	Poor	53	70	80	85
	Fair	40	63	75	81
	Good	31	57	71	78
Chaparral, Narrowleaf (Chamise and redshank)	Poor	71	82	88	91
	Fair	55	72	81	86
Grass, Annual or Perennial	Poor	67	78	86	89
	Fair	50	69	79	84
	Good	38	61	74	80
Meadows or Cienegas (Areas with seasonally high water table, principal vegetation is sod forming grass)	Poor	63	77	85	88
	Fair	51	70	80	84
	Good	30	58	71	78
Open Brush (Soft wood shrubs - buckwheat, sage, etc.)	Poor	62	76	84	88
	Fair	46	66	77	83
	Good	41	63	75	81
Woodland (Coniferous or broadleaf trees predominate. Canopy density is at least 50 percent.)	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	25	55	70	77
Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)	Poor	57	73	82	86
	Fair	44	65	77	82
	Good	33	58	72	79
<u>URBAN COVERS -</u>					
Residential or Commercial Landscaping (Lawn, shrubs, etc.)	Good	32	56	69	75
Turf (Irrigated and mowed grass)	Poor	58	74	83	87
	Fair	44	65	77	82
	Good	33	58	72	79
<u>AGRICULTURAL COVERS -</u>					
Fallow (Land plowed but not tilled or seeded)		77	86	91	94
SAN BERNARDINO COUNTY		CURVE NUMBERS			
HYDROLOGY MANUAL		FOR			
		PERVIOUS AREAS			

ACTUAL IMPERVIOUS COVER		
Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent (2)
Natural or Agriculture	0 - 0	0
Public Park	10 - 25	15
School	30 - 50	40
Single Family Residential: (3)		
2.5 acre lots	5 - 15	10
1 acre lots	10 - 25	20
2 dwellings/acre	20 - 40	30
3-4 dwellings/acre	30 - 50	40
5-7 dwellings/acre	35 - 55	50
8-10 dwellings/acre	50 - 70	60
More than 10 dwellings/acre	65 - 90	80
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 - 100	90

Notes:

1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.
2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area shall always be made, and a review of aerial photos, where available, may assist in estimating the percentage of impervious cover in developed areas.
3. For typical equestrian subdivisions increase impervious area 5 percent over the values recommended in the table above.

SAN BERNARDINO COUNTY
HYDROLOGY MANUAL

**ACTUAL IMPERVIOUS COVER
FOR
DEVELOPED AREAS**

HYDRAULICS

Storm Drain System Calculations

Open Channel, Pipe and Inlet program Flow Master by Haestad Methods, Reference 7 was used to determine the street capacity, ditch capacity and inlet sizing.

Main line system: the following assumptions and criteria were used to design the main line system:

1. $n = 0.013$ for reinforced concrete pipe, $n = 0.014$ for reinforced concrete box, and $n = 0.015$ for concrete V-ditch.
2. The minor losses considered in this study are as follows: friction loss, junction loss, transition loss, and manhole loss. In order to minimize junction structure losses, all junctions are inletting the main line at an angle of approximately 45 degrees.

Preliminary pipe sizing were determined by using full flow pipe capacity. When storm drain system profile is available then WSPG will be used to determine Hydraulic Grade Line of the proposed storm drain system.

See below calculations:

Rating Table for Circular Pipe - with slope 0.01

Project Description

Friction Method Manning Formula
Solve For Full Flow Capacity

Input Data

Roughness Coefficient 0.013
Channel Slope 0.01000 ft/ft
Normal Depth 4.00 ft
Diameter 4.00 ft
Discharge 143.64 ft³/s

Diameter (ft)	Normal Depth (ft)	Discharge (ft ³ /s)	Velocity (ft/s)	Flow Area (ft ²)	Wetted Perimeter (ft)	Top Width (ft)
1.50	1.50	10.50	5.94	1.77	4.71	0.00
2.00	2.00	22.62	7.20	3.14	6.28	0.00
2.50	2.50	41.01	8.36	4.91	7.85	0.00
3.00	3.00	66.69	9.44	7.07	9.42	0.00
3.50	3.50	100.60	10.46	9.62	11.00	0.00
4.00	4.00	143.64	11.43	12.57	12.57	0.00
4.50	4.50	196.64	12.36	15.90	14.14	0.00
5.00	5.00	260.43	13.26	19.63	15.71	0.00
5.50	5.50	335.79	14.13	23.76	17.28	0.00
6.00	6.00	423.49	14.98	28.27	18.85	0.00

Summary Mainline Storm Drain Pipe sizing based on 100-year storm:

Drainage Area	Area in Acre	Q ₁₀₀ sub-area in cfs	Q ₁₀₀ conf. in cfs	Estimate Mainline Pipe size (dia. in inches)
A-1	5.70	15.96		24"
A-2	6.46	15.18	31.14	30"
A-3	5.40	10.63	41.77	
A-4	4.28	10.25	52.02	36"
A-5	3.84	7.32	59.34	36"
A-6	1.08	2.83	61.37	
A-7	4.47	12.32		24"
A-8	4.28	10.24	22.56	30"
A-9	1.15	5.04		
A-10	1.75	5.19	10.23	18"
		Node 105	88.39	42"
A-11	7.60	20.05		24"
		Node 111	105.73	42"
A-12	4.46	11.47		
A-13	6.96	18.24	29.70	
A-14	1.59	4.40	34.11	30"
A-15	7.23	13.62	47.72	36"
A-16	2.64	4.69	52.41	36"
A-17	3.57	8.08	60.50	36"
		Node 120	166.15	48"
B-1	4.88	12.39		24"
B-2	6.02	13.78	26.17	24"
B-3	10.20	24.49	50.65	36"
B-4	2.35	4.04	54.69	36"
C-1	3.13	10.86		18"
C-2	3.75	7.81	18.67	
C-3	4.12	10.40	29.08	30"
C-4	0.23	0.50	29.58	30"
D-1	2.24	7.03		18"
E-1	5.25	16.11		channel
E-2	11.80	32.61	48.72	channel
E-3	3.85	8.44	57.16	channel
E-4	5.88	13.42	70.57	channel
				36"
E-5	3.86	4.48	75.05	channel
E-6	3.85	9.43	84.48	42"
F-1	4.38	16.52		
F-2	4.54	17.12	33.64	30"
F-3	10.20	36.51	70.16	36"
F-4	1.29	4.08	74.24	42"

G-1	5.14	15.03		channel
G-2	5.32	14.06	29.10	channel
	1.00	2.97	32.07	30" culvert
G-3	25.60	71.21	103.27	channel
				42" culvert
G-4	17.80	45.03	148.30	channel
				48" culvert
G-5	2.53	6.19	154.50	
	1.00	2.88	157.37	channel
G-6	2.41	8.63		
G-7	9.05	28.77	37.40	30"
G-8	0.77	2.01	39.41	30"
		NODE 704	192.24	54" culvert
G-9	18.70	36.62	228.86	channel
G-10	8.80	22.34	251.20	channel
	2.00	5.46		channel
		NODE 705	256.66	channel
H-1	5.27	15.81		24"
I-1	4.10	13.11		
I-2	5.85	18.71	31.82	30"
I-3	12.41	39.13	70.95	36"

Rating Table for Trapezoidal Channel - Conc. Channel

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient 0.015
Channel Slope 0.0100 ft/ft
Left Side Slope 1.50 ft/ft (H:V)
Right Side Slope 1.50 ft/ft (H:V)
Bottom Width 3.00 ft
Discharge 50.00 ft³/s

Channel Slope (ft/ft)					Wetted Perimeter (ft)	
	Bottom Width (ft)	Normal Depth (ft)	Velocity (ft/s)	Flow Area (ft ²)	Top Width (ft)	
0.0100	1.00	1.65	8.71	5.74	6.95	5.95
0.0100	1.50	1.52	8.70	5.75	6.98	6.06
0.0100	2.00	1.41	8.66	5.77	7.07	6.22
0.0100	2.50	1.31	8.59	5.82	7.21	6.42
0.0100	3.00	1.22	8.50	5.88	7.39	6.65
0.0100	3.50	1.14	8.40	5.95	7.62	6.92
0.0100	4.00	1.07	8.29	6.03	7.87	7.22
0.0150	1.00	1.51	10.15	4.93	6.44	5.53
0.0150	1.50	1.38	10.12	4.94	6.48	5.65
0.0150	2.00	1.27	10.06	4.97	6.59	5.82
0.0150	2.50	1.18	9.96	5.02	6.74	6.03
0.0150	3.00	1.09	9.85	5.08	6.95	6.28
0.0150	3.50	1.02	9.71	5.15	7.19	6.57
0.0150	4.00	0.96	9.57	5.22	7.46	6.88
0.0200	1.00	1.42	11.30	4.42	6.11	5.25
0.0200	1.50	1.29	11.26	4.44	6.16	5.37
0.0200	2.00	1.18	11.18	4.47	6.27	5.55
0.0200	2.50	1.09	11.06	4.52	6.44	5.78
0.0200	3.00	1.01	10.92	4.58	6.65	6.04
0.0200	3.50	0.95	10.76	4.65	6.91	6.34
0.0200	4.00	0.89	10.59	4.72	7.20	6.66
0.0250	1.00	1.35	12.29	4.07	5.86	5.04
0.0250	1.50	1.22	12.24	4.09	5.91	5.17
0.0250	2.00	1.12	12.14	4.12	6.04	5.36
0.0250	2.50	1.03	12.00	4.17	6.21	5.59
0.0250	3.00	0.95	11.83	4.23	6.44	5.86
0.0250	3.50	0.89	11.64	4.29	6.70	6.17
0.0250	4.00	0.83	11.44	4.37	7.00	6.50
0.0300	1.00	1.29	13.15	3.80	5.66	4.88
0.0300	1.50	1.17	13.09	3.82	5.73	5.02
0.0300	2.00	1.07	12.98	3.85	5.85	5.21
0.0300	2.50	0.98	12.82	3.90	6.04	5.45
0.0300	3.00	0.91	12.63	3.96	6.27	5.72

0.0300	3.50	0.84	12.41	4.03	6.55	6.03
0.0300	4.00	0.79	12.19	4.10	6.85	6.37
0.0350	1.00	1.25	13.93	3.59	5.50	4.75
0.0350	1.50	1.13	13.87	3.61	5.57	4.89
0.0350	2.00	1.03	13.73	3.64	5.71	5.08
0.0350	2.50	0.94	13.56	3.69	5.90	5.33
0.0350	3.00	0.87	13.34	3.75	6.14	5.61
0.0350	3.50	0.81	13.11	3.81	6.42	5.93
0.0350	4.00	0.76	12.86	3.89	6.73	6.27
0.0400	1.00	1.21	14.65	3.41	5.37	4.63
0.0400	1.50	1.09	14.57	3.43	5.44	4.78
0.0400	2.00	0.99	14.43	3.47	5.58	4.98
0.0400	2.50	0.91	14.23	3.51	5.78	5.23
0.0400	3.00	0.84	13.99	3.57	6.03	5.52
0.0400	3.50	0.78	13.73	3.64	6.31	5.84
0.0400	4.00	0.73	13.46	3.71	6.63	6.19
0.0450	1.00	1.18	15.31	3.27	5.25	4.54
0.0450	1.50	1.06	15.22	3.29	5.33	4.69
0.0450	2.00	0.96	15.05	3.32	5.48	4.89
0.0450	2.50	0.88	14.84	3.37	5.68	5.15
0.0450	3.00	0.81	14.58	3.43	5.93	5.44
0.0450	3.50	0.75	14.31	3.49	6.22	5.76
0.0450	4.00	0.70	14.03	3.57	6.54	6.11
0.0500	1.00	1.15	15.92	3.14	5.15	4.45
0.0500	1.50	1.04	15.83	3.16	5.23	4.61
0.0500	2.00	0.94	15.64	3.20	5.38	4.81
0.0500	2.50	0.86	15.42	3.24	5.59	5.07
0.0500	3.00	0.79	15.14	3.30	5.85	5.37
0.0500	3.50	0.73	14.84	3.37	6.14	5.70
0.0500	4.00	0.68	14.53	3.44	6.47	6.05

CONCLUSIONS

The proposed project grading areas and proposed drainage systems are in conformance with Specific Plan, Drainage Master Plan and proposed Land Use. The proposed grading and the proposed storm drain system will connect to existing facilities where it is reasonably feasible, and/or outlet to existing drainage facilities. Potential project impacts related to drainage runoff and water quality will be mitigated according to County/City requirements.

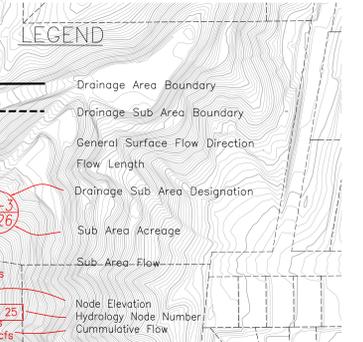
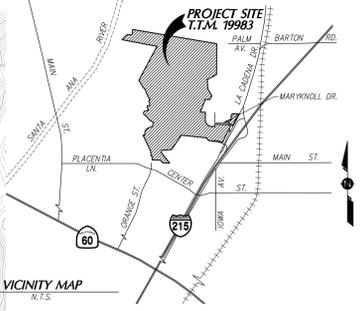
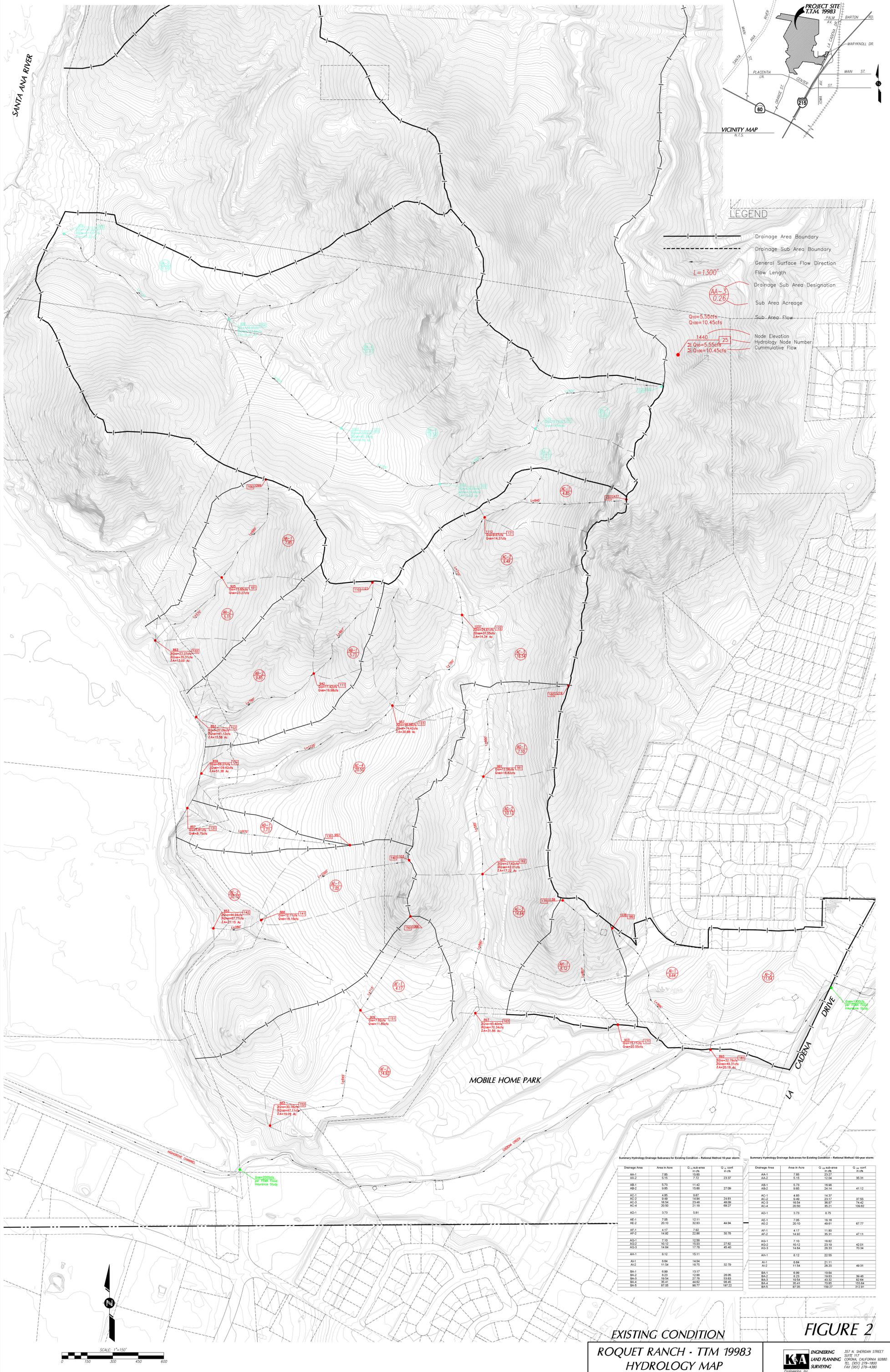
The proposed backbone storm drain systems are designed for ultimate / proposed condition for 100-year storm event. A final report will be prepared to accurately document the catch basin sizing, storm drain water surface profile as well as storm drain system to include water quality BMPs to make sure that the system capable to pass the 100 year event and the various water quality BMPs mitigation currently proposed through the City review and approval process.

REFERENCES

1. County of San Bernardino County Hydrology Manual, August 1986, as incorporated in the Civildesign Rational Method Hydrology Software.
2. CivilCADD/Design Engineering Software, version 7.1.
3. Roquet Ranch Tentative Tract Map 19983.
4. WSPG, Los Angeles County Public Works Water Surface Profile software - Storm Drain Analysis Plus by CivilSoft.
5. Hydraulic Calculations software by Haestad Method, Inc., Flow Master V6.0

FIGURES

FIGURE 2
Hydrology Map – Existing Condition



Summary Hydrology Drainage Sub-areas for Existing Condition - Rational Method 10-year storm

Drainage Area	Area in Acres	Q ₁₀ in cfs	Q ₁₀ in cfs
AA-1	7.85	15.85	23.37
AA-2	5.15	7.72	23.37
AB-1	5.73	11.22	27.89
AB-2	9.85	19.88	48.69
AC-1	4.85	9.67	24.61
AC-2	9.69	19.34	49.22
AC-3	16.54	33.08	82.27
AC-4	20.50	41.00	102.27
AD-1	3.73	5.81	14.78
AE-1	7.85	15.85	40.44
AE-2	20.10	39.83	100.11
AF-1	4.17	7.92	20.11
AF-2	14.88	29.86	76.28
AG-1	7.10	13.98	35.85
AG-2	10.17	19.93	51.85
AG-3	14.84	29.68	76.28
AH-1	8.12	16.11	41.78
AH-2	8.84	17.68	45.46
AH-3	11.54	23.08	59.71
AI-1	6.99	13.97	35.85
AI-2	8.23	16.46	42.15
AI-3	10.54	21.08	54.21
AI-4	16.46	32.92	84.60
AI-5	87.05	174.10	445.26

Summary Hydrology Drainage Sub-areas for Existing Condition - Rational Method 100-year storm

Drainage Area	Area in Acres	Q ₁₀₀ in cfs	Q ₁₀₀ in cfs
AA-1	7.85	15.85	23.37
AA-2	5.15	7.72	23.37
AB-1	5.73	11.22	27.89
AB-2	9.85	19.88	48.69
AC-1	4.85	9.67	24.61
AC-2	9.69	19.34	49.22
AC-3	16.54	33.08	82.27
AC-4	20.50	41.00	102.27
AD-1	3.73	5.81	14.78
AE-1	7.85	15.85	40.44
AE-2	20.10	39.83	100.11
AF-1	4.17	7.92	20.11
AF-2	14.88	29.86	76.28
AG-1	7.10	13.98	35.85
AG-2	10.17	19.93	51.85
AG-3	14.84	29.68	76.28
AH-1	8.12	16.11	41.78
AH-2	8.84	17.68	45.46
AH-3	11.54	23.08	59.71
AI-1	6.99	13.97	35.85
AI-2	8.23	16.46	42.15
AI-3	10.54	21.08	54.21
AI-4	16.46	32.92	84.60
AI-5	87.05	174.10	445.26

EXISTING CONDITION
ROQUET RANCH - TTM 19983
HYDROLOGY MAP

FIGURE 2

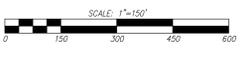
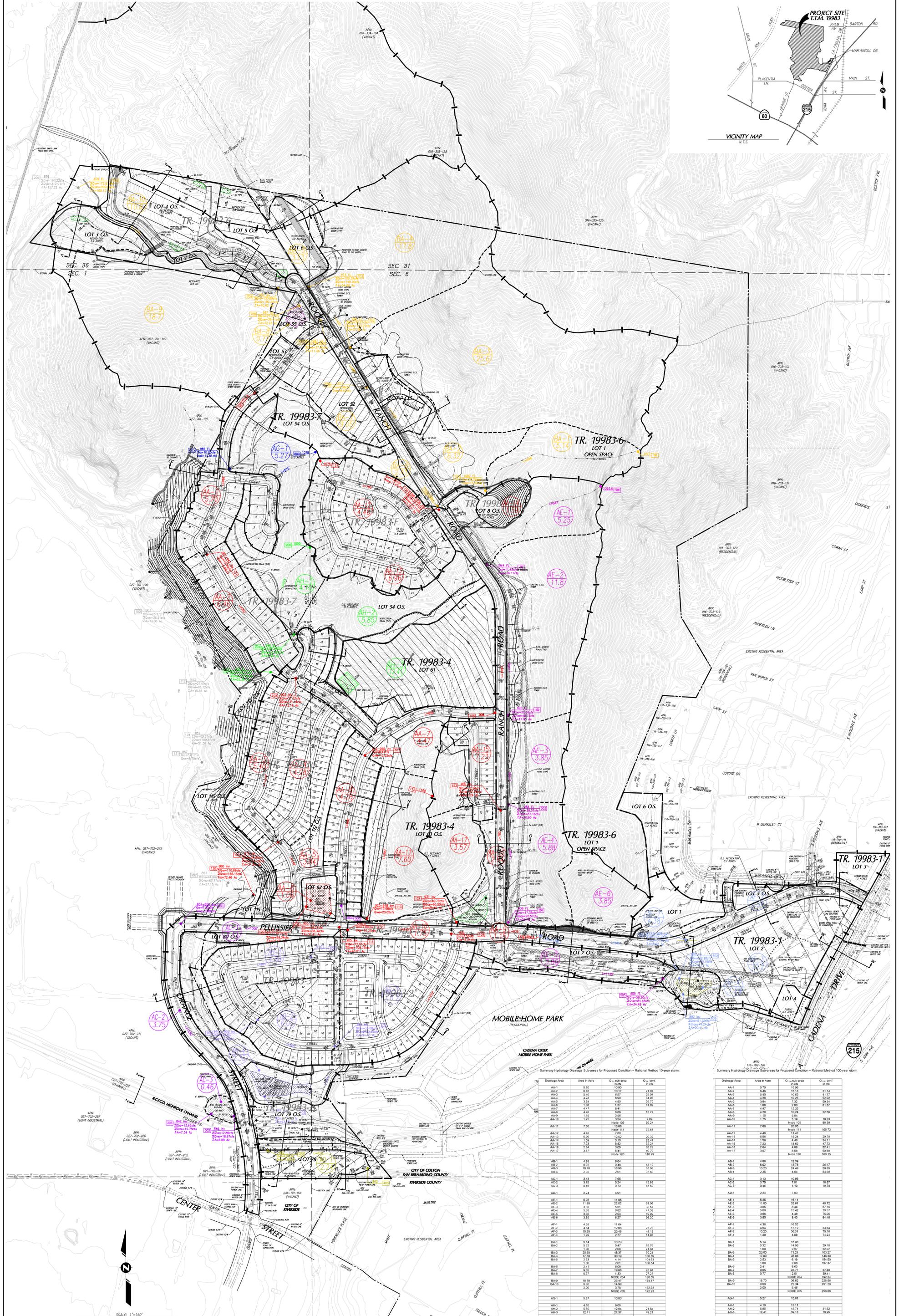
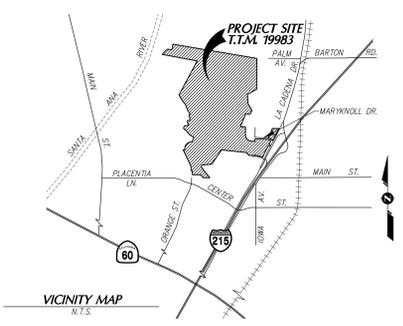


FIGURE 3
Hydrology Map - Proposed Condition



Summary Hydrology Drainage Sub-areas for Proposed Condition - Rational Method 10 year storm.

Drainage Area	Area in Acres	Q ₁₀ in cfs	Q ₁₀ in cfs
BA-1	5.78	10.90	21.07
BA-2	6.49	10.17	21.07
BA-3	4.39	6.90	34.95
BA-4	2.64	4.40	21.02
BA-5	1.09	1.77	21.02
BA-6	4.47	4.41	21.02
BA-7	4.38	6.98	15.27
BA-8	1.10	3.08	15.24
BA-9	1.75	3.54	7.90
BA-10	1.75	3.54	15.24
Notes 150			
AA-11	7.60	13.95	17.61
AA-12	4.48	7.80	30.32
AA-13	8.96	15.62	30.32
AA-14	1.79	3.10	32.41
AA-15	10.20	29.48	32.24
AA-16	2.64	3.05	30.39
AA-17	3.57	5.41	30.70
Notes 120			
AB-1	2.88	9.48	18.12
AB-2	6.02	9.48	18.12
AB-3	12.20	18.96	37.68
AB-4	2.30	2.61	37.68
Notes 120			
AC-1	3.13	7.65	13.86
AC-2	3.78	8.54	13.86
AC-3	0.46	0.73	13.82
Notes 120			
AD-1	2.24	4.91	
Notes 111			
AE-1	5.35	11.85	33.06
AE-2	11.80	22.02	33.06
AE-3	3.85	5.61	33.07
AE-4	7.88	8.62	37.38
AE-5	3.88	2.54	49.92
AE-6	3.85	4.27	49.92
Notes 100			
AF-1	4.38	11.64	
AF-2	4.54	12.06	23.70
AF-3	10.20	29.48	23.70
AF-4	1.29	2.77	31.95
Notes 100			
BA-1	5.14	10.29	19.78
BA-2	5.52	9.47	21.21
BA-3	35.00	48.37	33.01
BA-4	1.82	3.64	33.01
BA-5	2.58	4.14	104.53
BA-6	1.82	3.64	104.54
BA-7	2.41	6.09	19.84
BA-8	4.88	10.54	19.84
BA-9	0.77	1.53	37.27
Notes 100			
BA-9	18.70	33.47	134.17
BA-10	8.92	14.88	134.17
BA-11	2.00	3.78	173.03
BA-12	12.41	27.37	173.03
Notes 100			
AG-1	5.27	10.63	
AH-1	4.10	9.00	
AH-2	5.95	12.84	21.84
AH-3	12.41	27.37	28.21

Summary Hydrology Drainage Sub-areas for Proposed Condition - Rational Method 100 year storm.

Drainage Area	Area in Acres	Q ₁₀₀ in cfs	Q ₁₀₀ in cfs
BA-1	5.78	5.30	31.14
BA-2	6.49	15.18	41.17
BA-3	4.39	10.25	52.52
BA-4	2.64	7.32	52.54
BA-5	1.09	2.03	61.37
BA-6	4.47	5.92	52.54
BA-7	4.38	10.24	22.56
BA-8	1.10	3.04	19.29
BA-9	1.75	3.19	10.23
BA-10	1.75	3.19	19.29
Notes 120			
AA-11	7.60	10.05	105.73
AA-12	4.48	11.47	105.73
AA-13	8.96	22.94	29.70
AA-14	1.79	4.40	34.11
AA-15	10.20	27.92	47.72
AA-16	2.64	4.69	52.41
AA-17	3.57	5.87	60.70
Notes 120			
AB-1	2.88	9.26	18.15
AB-2	6.02	15.78	28.17
AB-3	12.20	24.96	56.34
AB-4	2.30	4.04	54.69
Notes 120			
AC-1	3.13	10.86	18.67
AC-2	3.78	12.01	18.67
AC-3	0.46	1.10	19.78
Notes 120			
AD-1	2.24	7.03	
Notes 111			
AE-1	5.35	16.11	48.72
AE-2	11.80	32.81	52.57
AE-3	3.85	8.44	70.16
AE-4	7.88	12.42	70.16
AE-5	3.88	4.48	75.05
AE-6	3.85	5.43	84.49
Notes 100			
AF-1	4.38	16.62	
AF-2	4.54	17.12	33.64
AF-3	10.20	36.61	70.16
AF-4	1.29	4.08	74.24
Notes 100			
BA-1	5.14	10.03	29.10
BA-2	5.52	9.59	31.57
BA-3	35.00	48.37	103.07
BA-4	1.82	3.64	103.07
BA-5	2.58	4.14	154.50
BA-6	1.82	3.64	154.50
BA-7	2.41	6.09	37.40
BA-8	4.88	10.54	37.40
BA-9	0.77	1.53	84.41
Notes 100			
BA-9	18.70	34.82	226.96
BA-10	8.92	22.44	226.96
BA-11	2.00	3.46	241.50
BA-12	12.41	27.37	241.50
Notes 100			
AG-1	5.27	15.81	
AH-1	4.10	13.11	
AH-2	5.95	18.71	31.62
AH-3	12.41	38.13	39.86

PROPOSED CONDITION
ROQUET RANCH - TTM 19983
HYDROLOGY MAP

FIGURE 3

ATTACHMENTS

ATTACHMENT A
Rational Method Hydrology
Existing Condition
(10 Year & 100 Year storm)

ATTACHMENT A
Rational Method Hydrology
Existing Condition
(10-Year storm)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2005 Version 7.1
Rational Hydrology Study Date: 02/10/16

Roquet Ranch Project
Existing Condition
10-year storm

Program License Serial Number 4029

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 10.0
Computed rainfall intensity:
Storm year = 10.00 1 hour rainfall = 0.850 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

+++++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 660.000(Ft.)
Top (of initial area) elevation = 1099.000(Ft.)
Bottom (of initial area) elevation = 925.000(Ft.)
Difference in elevation = 174.000(Ft.)
Slope = 0.26364 s(%)= 26.36
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.200 min.
Rainfall intensity = 2.618(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.761
Subarea runoff = 15.649(CFS)
Total initial stream area = 7.850(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.404(In/Hr)

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
Depth of flow = 0.423(Ft.), Average velocity = 6.649(Ft/s)
***** Irregular Channel Data *****

Information entered for subchannel number 1 :
Point number 'X' coordinate 'Y' coordinate

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

1	0.00	5.00
2	20.00	0.00
3	25.00	0.00
4	51.00	5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 19.553 (CFS)
 ' ' flow top width = 8.894 (Ft.)
 ' ' velocity = 6.649 (Ft/s)
 ' ' area = 2.941 (Sq.Ft)
 ' ' Froude number = 2.038

Upstream point elevation = 925.000 (Ft.)
 Downstream point elevation = 863.000 (Ft.)
 Flow length = 570.000 (Ft.)
 Travel time = 1.43 min.
 Time of concentration = 10.63 min.
 Depth of flow = 0.423 (Ft.)
 Average velocity = 6.649 (Ft/s)
 Total irregular channel flow = 19.553 (CFS)
 Irregular channel normal depth above invert elev. = 0.423 (Ft.)
 Average velocity of channel(s) = 6.649 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.401 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.749
 Subarea runoff = 7.724 (CFS) for 5.150 (Ac.)
 Total runoff = 23.373 (CFS)
 Effective area this stream = 13.00 (Ac.)
 Total Study Area (Main Stream No. 1) = 13.00 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.466 (Ft.), Average velocity = 7.016 (Ft/s)

+++++
 Process from Point/Station 110.000 to Point/Station 111.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 667.000 (Ft.)
 Top (of initial area) elevation = 1121.000 (Ft.)
 Bottom (of initial area) elevation = 942.000 (Ft.)
 Difference in elevation = 179.000 (Ft.)
 Slope = 0.26837 s(%) = 26.84
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 9.206 min.
 Rainfall intensity = 2.617 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.761
 Subarea runoff = 11.417 (CFS)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Total initial stream area = 5.730 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

+++++
 Process from Point/Station 111.000 to Point/Station 112.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.456 (Ft.), Average velocity = 6.844 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 22.00 0.00
 3 26.00 0.00
 4 52.00 5.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 19.290 (CFS)
 ' ' flow top width = 8.373 (Ft.)
 ' ' velocity = 6.844 (Ft/s)
 ' ' area = 2.818 (Sq.Ft)
 ' ' Froude number = 2.079

Upstream point elevation = 942.000 (Ft.)
 Downstream point elevation = 853.000 (Ft.)
 Flow length = 790.000 (Ft.)
 Travel time = 1.92 min.
 Time of concentration = 11.13 min.
 Depth of flow = 0.456 (Ft.)
 Average velocity = 6.844 (Ft/s)
 Total irregular channel flow = 19.290 (CFS)
 Irregular channel normal depth above invert elev. = 0.456 (Ft.)
 Average velocity of channel(s) = 6.844 (Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.336 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.745
 Subarea runoff = 15.676 (CFS) for 9.850 (Ac.)
 Total runoff = 27.093 (CFS)
 Effective area this stream = 15.58 (Ac.)
 Total Study Area (Main Stream No. 1) = 28.58 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.544 (Ft.), Average velocity = 7.542 (Ft/s)

+++++
 Process from Point/Station 120.000 to Point/Station 121.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 845.000(Ft.)
 Top (of initial area) elevation = 1477.000(Ft.)
 Bottom (of initial area) elevation = 1112.000(Ft.)
 Difference in elevation = 365.000(Ft.)
 Slope = 0.43195 s(%)= 43.20
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.201 min.
 Rainfall intensity = 2.618(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.761
 Subarea runoff = 9.668(CFS)
 Total initial stream area = 4.850(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 121.000 to Point/Station 122.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.280(Ft.), Average velocity = 5.542(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	15.00	0.00
3	25.00	0.00
4	40.00	4.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 17.174(CFS)
 ' ' flow top width = 12.103(Ft.)
 ' ' velocity= 5.542(Ft/s)
 ' ' area = 3.099(Sq.Ft)
 ' ' Froude number = 1.930

Upstream point elevation = 1112.000(Ft.)
 Downstream point elevation = 1037.000(Ft.)
 Flow length = 710.000(Ft.)
 Travel time = 2.14 min.
 Time of concentration = 11.34 min.
 Depth of flow = 0.280(Ft.)
 Average velocity = 5.542(Ft/s)
 Total irregular channel flow = 17.174(CFS)
 Irregular channel normal depth above invert elev. = 0.280(Ft.)
 Average velocity of channel(s) = 5.542(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.310(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.743

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Subarea runoff = 14.939(CFS) for 9.490 (Ac.)
 Total runoff = 24.607(CFS)
 Effective area this stream = 14.34(Ac.)
 Total Study Area (Main Stream No. 1) = 42.92(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.346(Ft.), Average velocity = 6.295(Ft/s)

++++
 Process from Point/Station 122.000 to Point/Station 123.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.595(Ft.), Average velocity = 7.900(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 20.00 0.00
 3 25.00 0.00
 4 51.00 5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 36.390(CFS)
 ' ' flow top width = 10.477(Ft.)
 ' ' velocity= 7.900(Ft/s)
 ' ' area = 4.606(Sq.Ft)
 ' ' Froude number = 2.099

Upstream point elevation = 1037.000(Ft.)
 Downstream point elevation = 957.000(Ft.)
 Flow length = 760.000(Ft.)
 Travel time = 1.60 min.
 Time of concentration = 12.94 min.
 Depth of flow = 0.595(Ft.)
 Average velocity = 7.900(Ft/s)
 Total irregular channel flow = 36.390(CFS)
 Irregular channel normal depth above invert elev. = 0.595(Ft.)
 Average velocity of channel(s) = 7.900(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.134(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.730
 Subarea runoff = 23.483(CFS) for 16.540(Ac.)
 Total runoff = 48.089(CFS)
 Effective area this stream = 30.88(Ac.)
 Total Study Area (Main Stream No. 1) = 59.46(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.688(Ft.), Average velocity = 8.556(Ft/s)

++++
 Process from Point/Station 123.000 to Point/Station 124.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.611 (Ft.), Average velocity = 7.506 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 6.00
 2 25.00 0.00
 3 35.00 0.00
 4 65.00 6.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 58.726 (CFS)
 ' ' flow top width = 15.602 (Ft.)
 ' ' velocity = 7.506 (Ft/s)
 ' ' area = 7.824 (Sq.Ft)
 ' ' Froude number = 1.868

Upstream point elevation = 957.000 (Ft.)
 Downstream point elevation = 859.000 (Ft.)
 Flow length = 1235.000 (Ft.)
 Travel time = 2.74 min.
 Time of concentration = 15.68 min.
 Depth of flow = 0.611 (Ft.)
 Average velocity = 7.506 (Ft/s)
 Total irregular channel flow = 58.726 (CFS)
 Irregular channel normal depth above invert elev. = 0.611 (Ft.)
 Average velocity of channel(s) = 7.506 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 1.901 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.709
 Subarea runoff = 21.177 (CFS) for 20.500 (Ac.)
 Total runoff = 69.266 (CFS)
 Effective area this stream = 51.38 (Ac.)
 Total Study Area (Main Stream No. 1) = 79.96 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.670 (Ft.), Average velocity = 7.909 (Ft/s)

++++
 Process from Point/Station 130.000 to Point/Station 131.000
 **** INITIAL AREA EVALUATION ****

 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 970.000 (Ft.)
 Top (of initial area) elevation = 957.000 (Ft.)
 Bottom (of initial area) elevation = 857.000 (Ft.)
 Difference in elevation = 100.000 (Ft.)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Slope = 0.10309 s(%)= 10.31
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 12.949 min.
 Rainfall intensity = 2.133(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.730
 Subarea runoff = 5.806(CFS)
 Total initial stream area = 3.730(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 140.000 to Point/Station 141.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 888.000(Ft.)
 Difference in elevation = 215.000(Ft.)
 Slope = 0.21500 s(%)= 21.50
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 11.315 min.
 Rainfall intensity = 2.313(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.743
 Subarea runoff = 12.113(CFS)
 Total initial stream area = 7.050(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 141.000 to Point/Station 142.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.501(Ft.), Average velocity = 7.848(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	20.00	0.00
3	25.00	0.00
4	50.00	5.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 28.554(CFS)
 ' ' flow top width = 9.513(Ft.)
 ' ' velocity= 7.848(Ft/s)
 ' ' area = 3.638(Sq.Ft)
 ' ' Froude number = 2.236

Upstream point elevation = 888.000(Ft.)
 Downstream point elevation = 853.000(Ft.)
 Flow length = 280.000(Ft.)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Travel time = 0.59 min.
 Time of concentration = 11.91 min.
 Depth of flow = 0.501(Ft.)
 Average velocity = 7.848(Ft/s)
 Total irregular channel flow = 28.554(CFS)
 Irregular channel normal depth above invert elev. = 0.501(Ft.)
 Average velocity of channel(s) = 7.848(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.243(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.738
 Subarea runoff = 32.826(CFS) for 20.100(Ac.)
 Total runoff = 44.939(CFS)
 Effective area this stream = 27.15(Ac.)
 Total Study Area (Main Stream No. 1) = 110.84(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.637(Ft.), Average velocity = 8.959(Ft/s)

++++++
 Process from Point/Station 150.000 to Point/Station 151.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 715.000(Ft.)
 Top (of initial area) elevation = 1066.000(Ft.)
 Bottom (of initial area) elevation = 909.000(Ft.)
 Difference in elevation = 157.000(Ft.)
 Slope = 0.21958 s(%) = 21.96
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.853 min.
 Rainfall intensity = 2.513(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 7.916(CFS)
 Total initial stream area = 4.170(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 151.000 to Point/Station 152.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.540(Ft.), Average velocity = 5.650(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

1	0.00	4.00
2	15.00	0.00
3	20.00	0.00
4	25.00	4.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 19.373 (CFS)
 ' ' flow top width = 7.700 (Ft.)
 ' ' velocity = 5.650 (Ft/s)
 ' ' area = 3.429 (Sq.Ft)
 ' ' Froude number = 1.492

Upstream point elevation = 909.000 (Ft.)
 Downstream point elevation = 863.000 (Ft.)
 Flow length = 845.000 (Ft.)
 Travel time = 2.49 min.
 Time of concentration = 12.35 min.
 Depth of flow = 0.540 (Ft.)
 Average velocity = 5.650 (Ft/s)
 Total irregular channel flow = 19.373 (CFS)
 Irregular channel normal depth above invert elev. = 0.540 (Ft.)
 Average velocity of channel(s) = 5.650 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.195 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.735
 Subarea runoff = 22.860 (CFS) for 14.920 (Ac.)
 Total runoff = 30.777 (CFS)
 Effective area this stream = 19.09 (Ac.)
 Total Study Area (Main Stream No. 1) = 129.93 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.699 (Ft.), Average velocity = 6.522 (Ft/s)

+++++
 Process from Point/Station 160.000 to Point/Station 161.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 950.000 (Ft.)
 Top (of initial area) elevation = 1219.000 (Ft.)
 Bottom (of initial area) elevation = 991.000 (Ft.)
 Difference in elevation = 228.000 (Ft.)
 Slope = 0.24000 s(%) = 24.00
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 10.844 min.
 Rainfall intensity = 2.372 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.747
 Subarea runoff = 12.581 (CFS)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Total initial stream area = 7.100 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

+++++
 Process from Point/Station 161.000 to Point/Station 162.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.537 (Ft.), Average velocity = 5.920 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 4.00
 2 15.00 0.00
 3 20.00 0.00
 4 25.00 4.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 20.147 (CFS)
 ' ' flow top width = 7.683 (Ft.)
 ' ' velocity = 5.920 (Ft/s)
 ' ' area = 3.403 (Sq.Ft)
 ' ' Froude number = 1.568

Upstream point elevation = 991.000 (Ft.)
 Downstream point elevation = 957.000 (Ft.)
 Flow length = 565.000 (Ft.)
 Travel time = 1.59 min.
 Time of concentration = 12.44 min.
 Depth of flow = 0.537 (Ft.)
 Average velocity = 5.920 (Ft/s)
 Total irregular channel flow = 20.147 (CFS)
 Irregular channel normal depth above invert elev. = 0.537 (Ft.)
 Average velocity of channel(s) = 5.920 (Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.185 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.734
 Subarea runoff = 15.034 (CFS) for 10.120 (Ac.)
 Total runoff = 27.615 (CFS)
 Effective area this stream = 17.22 (Ac.)
 Total Study Area (Main Stream No. 1) = 147.15 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.640 (Ft.), Average velocity = 6.532 (Ft/s)

+++++
 Process from Point/Station 162.000 to Point/Station 163.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.661 (Ft.), Average velocity = 6.933 (Ft/s)
 ***** Irregular Channel Data *****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

```

-----
Information entered for subchannel number 1 :
Point number      'X' coordinate      'Y' coordinate
      1              0.00              5.00
      2             20.00              0.00
      3             25.00              0.00
      4             50.00              5.00
Manning's 'N' friction factor = 0.035
-----

```

```

-----
Sub-Channel flow = 36.556(CFS)
'   '   flow top width = 10.950(Ft.)
'   '   velocity= 6.933(Ft/s)
'   '   area = 5.273(Sq.Ft)
'   '   Froude number = 1.761
-----

```

```

Upstream point elevation = 957.000(Ft.)
Downstream point elevation = 893.000(Ft.)
Flow length = 890.000(Ft.)
Travel time = 2.14 min.
Time of concentration = 14.57 min.
Depth of flow = 0.661(Ft.)
Average velocity = 6.933(Ft/s)
Total irregular channel flow = 36.556(CFS)
Irregular channel normal depth above invert elev. = 0.661(Ft.)
Average velocity of channel(s) = 6.933(Ft/s)
Adding area flow to channel

```

```

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Rainfall intensity = 1.987(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.717
Subarea runoff = 17.784(CFS) for 14.640(Ac.)
Total runoff = 45.399(CFS)
Effective area this stream = 31.86(Ac.)
Total Study Area (Main Stream No. 1) = 161.79(Ac.)
Area averaged Fm value = 0.404(In/Hr)
Depth of flow = 0.739(Ft.), Average velocity = 7.372(Ft/s)

```

```

+++++
Process from Point/Station 170.000 to Point/Station 171.000
**** INITIAL AREA EVALUATION ****

```

```

-----
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 857.000(Ft.)
Top (of initial area) elevation = 1138.000(Ft.)
Bottom (of initial area) elevation = 903.000(Ft.)
Difference in elevation = 235.000(Ft.)
Slope = 0.27421 s(%)= 27.42
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.133 min.

```

Roquet Ranch (TTM 19982) – Drainage Report
ATTACHMENT A

Rainfall intensity = 2.471(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.753
Subarea runoff = 15.109(CFS)
Total initial stream area = 8.120(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.404(In/Hr)

+++++
Process from Point/Station 180.000 to Point/Station 181.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 996.000(Ft.)
Top (of initial area) elevation = 1038.000(Ft.)
Bottom (of initial area) elevation = 893.000(Ft.)
Difference in elevation = 145.000(Ft.)
Slope = 0.14558 s(%)= 14.56
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 12.214 min.
Rainfall intensity = 2.209(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.736
Subarea runoff = 14.040(CFS)
Total initial stream area = 8.640(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.404(In/Hr)

+++++
Process from Point/Station 180.000 to Point/Station 181.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Time of concentration = 12.21 min.
Rainfall intensity = 2.209(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.736
Subarea runoff = 18.752(CFS) for 11.540(Ac.)
Total runoff = 32.792(CFS)
Effective area this stream = 20.18(Ac.)
Total Study Area (Main Stream No. 1) = 190.09(Ac.)
Area averaged Fm value = 0.404(In/Hr)

+++++
Process from Point/Station 200.000 to Point/Station 201.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 850.000(Ft.)
 Top (of initial area) elevation = 1422.000(Ft.)
 Bottom (of initial area) elevation = 1172.000(Ft.)
 Difference in elevation = 250.000(Ft.)
 Slope = 0.29412 s(%)= 29.41
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.959 min.
 Rainfall intensity = 2.497(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.755
 Subarea runoff = 13.169(CFS)
 Total initial stream area = 6.990(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+-----+
 Process from Point/Station 201.000 to Point/Station 202.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.387(Ft.), Average velocity = 8.185(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	15.00	0.00
3	20.00	0.00
4	30.00	4.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 19.653(CFS)
 ' ' flow top width = 7.417(Ft.)
 ' ' velocity= 8.185(Ft/s)
 ' ' area = 2.401(Sq.Ft)
 ' ' Froude number = 2.535

Upstream point elevation = 1172.000(Ft.)
 Downstream point elevation = 1053.000(Ft.)
 Flow length = 696.000(Ft.)
 Travel time = 1.42 min.
 Time of concentration = 11.38 min.
 Depth of flow = 0.387(Ft.)
 Average velocity = 8.185(Ft/s)
 Total irregular channel flow = 19.653(CFS)
 Irregular channel normal depth above invert elev. = 0.387(Ft.)
 Average velocity of channel(s) = 8.185(Ft/s)
 Adding area flow to channel

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.305(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

rational method) (Q=KCIA) is C = 0.742
 Subarea runoff = 12.881(CFS) for 8.230(Ac.)
 Total runoff = 26.049(CFS)
 Effective area this stream = 15.22(Ac.)
 Total Study Area (Main Stream No. 1) = 205.31(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.453(Ft.), Average velocity = 8.957(Ft/s)

++++
 Process from Point/Station 202.000 to Point/Station 203.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.695(Ft.), Average velocity = 7.077(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 20.00 0.00
 3 25.00 0.00
 4 50.00 5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 39.989(CFS)
 ' ' flow top width = 11.257(Ft.)
 ' ' velocity = 7.077(Ft/s)
 ' ' area = 5.651(Sq.Ft)
 ' ' Froude number = 1.760

Upstream point elevation = 1053.000(Ft.)
 Downstream point elevation = 1003.000(Ft.)
 Flow length = 705.000(Ft.)
 Travel time = 1.66 min.
 Time of concentration = 13.04 min.
 Depth of flow = 0.695(Ft.)
 Average velocity = 7.077(Ft/s)
 Total irregular channel flow = 39.989(CFS)
 Irregular channel normal depth above invert elev. = 0.695(Ft.)
 Average velocity of channel(s) = 7.077(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Rainfall intensity = 2.124(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.729
 Subarea runoff = 27.783(CFS) for 19.540(Ac.)
 Total runoff = 53.832(CFS)
 Effective area this stream = 34.76(Ac.)
 Total Study Area (Main Stream No. 1) = 224.85(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.810(Ft.), Average velocity = 7.694(Ft/s)

++++
 Process from Point/Station 203.000 to Point/Station 204.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.887 (Ft.), Average velocity = 8.601 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 6.00
 2 30.00 0.00
 3 36.00 0.00
 4 60.00 6.00

Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 76.185 (CFS)
 ' ' flow top width = 13.980 (Ft.)
 ' ' velocity = 8.601 (Ft/s)
 ' ' area = 8.857 (Sq.Ft)
 ' ' Froude number = 1.904

Upstream point elevation = 1003.000 (Ft.)
 Downstream point elevation = 930.000 (Ft.)
 Flow length = 950.000 (Ft.)
 Travel time = 1.84 min.
 Time of concentration = 14.88 min.
 Depth of flow = 0.887 (Ft.)
 Average velocity = 8.601 (Ft/s)
 Total irregular channel flow = 76.185 (CFS)
 Irregular channel normal depth above invert elev. = 0.887 (Ft.)
 Average velocity of channel(s) = 8.601 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 1.962 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.715
 Subarea runoff = 44.618 (CFS) for 35.410 (Ac.)
 Total runoff = 98.450 (CFS)
 Effective area this stream = 70.17 (Ac.)
 Total Study Area (Main Stream No. 1) = 260.26 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 1.010 (Ft.), Average velocity = 9.240 (Ft/s)

++++
 Process from Point/Station 204.000 to Point/Station 205.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 1.342 (Ft.), Average velocity = 8.451 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 7.00
 2 30.00 0.00
 3 37.00 0.00
 4 70.00 7.00

Manning's 'N' friction factor = 0.035

Roquet Ranch (TTM 19982) – Drainage Report
ATTACHMENT A

Sub-Channel flow = 147.861 (CFS)
' ' flow top width = 19.077 (Ft.)
' ' velocity = 8.451 (Ft/s)
' ' area = 17.497 (Sq.Ft)
' ' Froude number = 1.555

Upstream point elevation = 930.000 (Ft.)
Downstream point elevation = 876.000 (Ft.)
Flow length = 1190.000 (Ft.)
Travel time = 2.35 min.
Time of concentration = 17.22 min.
Depth of flow = 1.342 (Ft.)
Average velocity = 8.451 (Ft/s)
Total irregular channel flow = 147.861 (CFS)
Irregular channel normal depth above invert elev. = 1.342 (Ft.)
Average velocity of channel(s) = 8.451 (Ft/s)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 78.00
Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
Rainfall intensity = 1.797 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.698
Subarea runoff = 98.770 (CFS) for 87.050 (Ac.)
Total runoff = 197.219 (CFS)
Effective area this stream = 157.22 (Ac.)
Total Study Area (Main Stream No. 1) = 347.31 (Ac.)
Area averaged Fm value = 0.404 (In/Hr)
Depth of flow = 1.546 (Ft.), Average velocity = 9.137 (Ft/s)
End of computations, Total Study Area = 347.31 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction (Ap) = 1.000
Area averaged SCS curve number = 78.0

ATTACHMENT A
Rational Method Hydrology
Existing Condition
(100-Year storm)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2005 Version 7.1
Rational Hydrology Study Date: 02/10/16

Roquet Ranch Project
Existing Condition
100-year storm

Program License Serial Number 4029

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 100.0
Computed rainfall intensity:
Storm year = 100.00 1 hour rainfall = 1.200 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

+++++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 660.000(Ft.)
Top (of initial area) elevation = 1099.000(Ft.)
Bottom (of initial area) elevation = 925.000(Ft.)
Difference in elevation = 174.000(Ft.)
Slope = 0.26364 s(%)= 26.36
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.200 min.
Rainfall intensity = 3.697(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.802
Subarea runoff = 23.266(CFS)
Total initial stream area = 7.850(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.404(In/Hr)

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
Depth of flow = 0.526(Ft.), Average velocity = 7.504(Ft/s)
***** Irregular Channel Data *****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 20.00 0.00
 3 25.00 0.00
 4 51.00 5.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 29.315(CFS)
 ' ' flow top width = 9.843(Ft.)
 ' ' velocity= 7.504(Ft/s)
 ' ' area = 3.907(Sq.Ft)
 ' ' Froude number = 2.099

Upstream point elevation = 925.000(Ft.)
 Downstream point elevation = 863.000(Ft.)
 Flow length = 570.000(Ft.)
 Travel time = 1.27 min.
 Time of concentration = 10.47 min.
 Depth of flow = 0.526(Ft.)
 Average velocity = 7.504(Ft/s)
 Total irregular channel flow = 29.315(CFS)
 Irregular channel normal depth above invert elev. = 0.526(Ft.)
 Average velocity of channel(s) = 7.504(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.421(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.794
 Subarea runoff = 12.044(CFS) for 5.150(Ac.)
 Total runoff = 35.310(CFS)
 Effective area this stream = 13.00(Ac.)
 Total Study Area (Main Stream No. 1) = 13.00(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.581(Ft.), Average velocity = 7.923(Ft/s)

+++++
 Process from Point/Station 110.000 to Point/Station 111.000
 **** INITIAL AREA EVALUATION ****

 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 667.000(Ft.)
 Top (of initial area) elevation = 1121.000(Ft.)
 Bottom (of initial area) elevation = 942.000(Ft.)
 Difference in elevation = 179.000(Ft.)
 Slope = 0.26837 s(%)= 26.84
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 9.206 min.
 Rainfall intensity = 3.695(In/Hr) for a 100.0 year storm

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Effective runoff coefficient used for area (Q=KCIA) is C = 0.802
 Subarea runoff = 16.975 (CFS)
 Total initial stream area = 5.730 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

++++
 Process from Point/Station 111.000 to Point/Station 112.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.564 (Ft.), Average velocity = 7.694 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	22.00	0.00
3	26.00	0.00
4	52.00	5.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 29.090 (CFS)
 ' ' flow top width = 9.412 (Ft.)
 ' ' velocity = 7.694 (Ft/s)
 ' ' area = 3.781 (Sq.Ft)
 ' ' Froude number = 2.139

Upstream point elevation = 942.000 (Ft.)
 Downstream point elevation = 853.000 (Ft.)
 Flow length = 790.000 (Ft.)
 Travel time = 1.71 min.
 Time of concentration = 10.92 min.
 Depth of flow = 0.564 (Ft.)
 Average velocity = 7.694 (Ft/s)
 Total irregular channel flow = 29.090 (CFS)
 Irregular channel normal depth above invert elev. = 0.564 (Ft.)
 Average velocity of channel(s) = 7.694 (Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)
 Rainfall intensity = 3.336 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.791
 Subarea runoff = 24.142 (CFS) for 9.850 (Ac.)
 Total runoff = 41.117 (CFS)
 Effective area this stream = 15.58 (Ac.)
 Total Study Area (Main Stream No. 1) = 28.58 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.672 (Ft.), Average velocity = 8.472 (Ft/s)

++++
 Process from Point/Station 120.000 to Point/Station 121.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 845.000 (Ft.)
 Top (of initial area) elevation = 1477.000 (Ft.)
 Bottom (of initial area) elevation = 1112.000 (Ft.)
 Difference in elevation = 365.000 (Ft.)
 Slope = 0.43195 s(%)= 43.20
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.201 min.
 Rainfall intensity = 3.696 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.802
 Subarea runoff = 14.374 (CFS)
 Total initial stream area = 4.850 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

++++++
 Process from Point/Station 121.000 to Point/Station 122.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.357 (Ft.), Average velocity = 6.418 (Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	15.00	0.00
3	25.00	0.00
4	40.00	4.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 26.005 (CFS)
 ' ' flow top width = 12.680 (Ft.)
 ' ' velocity= 6.418 (Ft/s)
 ' ' area = 4.052 (Sq.Ft)
 ' ' Froude number = 2.001

Upstream point elevation = 1112.000 (Ft.)
 Downstream point elevation = 1037.000 (Ft.)
 Flow length = 710.000 (Ft.)
 Travel time = 1.84 min.
 Time of concentration = 11.04 min.
 Depth of flow = 0.357 (Ft.)
 Average velocity = 6.418 (Ft/s)
 Total irregular channel flow = 26.005 (CFS)
 Irregular channel normal depth above invert elev. = 0.357 (Ft.)
 Average velocity of channel(s) = 6.418 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)
 Rainfall intensity = 3.313 (In/Hr) for a 100.0 year storm

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.790
 Subarea runoff = 23.173(CFS) for 9.490(Ac.)
 Total runoff = 37.547(CFS)
 Effective area this stream = 14.34(Ac.)
 Total Study Area (Main Stream No. 1) = 42.92(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.442(Ft.), Average velocity = 7.286(Ft/s)

++++
 Process from Point/Station 122.000 to Point/Station 123.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

 Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.744(Ft.), Average velocity = 8.931(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 5.00
 2 20.00 0.00
 3 25.00 0.00
 4 51.00 5.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 56.009(CFS)
 ' ' flow top width = 11.848(Ft.)
 ' ' velocity = 8.932(Ft/s)
 ' ' area = 6.271(Sq.Ft)
 ' ' Froude number = 2.164

Upstream point elevation = 1037.000(Ft.)
 Downstream point elevation = 957.000(Ft.)
 Flow length = 760.000(Ft.)
 Travel time = 1.42 min.
 Time of concentration = 12.46 min.
 Depth of flow = 0.744(Ft.)
 Average velocity = 8.931(Ft/s)
 Total irregular channel flow = 56.009(CFS)
 Irregular channel normal depth above invert elev. = 0.744(Ft.)
 Average velocity of channel(s) = 8.931(Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.081(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.782
 Subarea runoff = 36.869(CFS) for 16.540(Ac.)
 Total runoff = 74.416(CFS)
 Effective area this stream = 30.88(Ac.)
 Total Study Area (Main Stream No. 1) = 59.46(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.860(Ft.), Average velocity = 9.666(Ft/s)

++++
 Process from Point/Station 123.000 to Point/Station 124.000

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

**** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.784 (Ft.), Average velocity = 8.639 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 6.00
 2 25.00 0.00
 3 35.00 0.00
 4 65.00 6.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 92.050 (CFS)
 ' ' flow top width = 17.186 (Ft.)
 ' ' velocity = 8.639 (Ft/s)
 ' ' area = 10.655 (Sq.Ft)
 ' ' Froude number = 1.934

Upstream point elevation = 957.000 (Ft.)
 Downstream point elevation = 859.000 (Ft.)
 Flow length = 1235.000 (Ft.)
 Travel time = 2.38 min.
 Time of concentration = 14.85 min.
 Depth of flow = 0.784 (Ft.)
 Average velocity = 8.639 (Ft/s)
 Total irregular channel flow = 92.050 (CFS)
 Irregular channel normal depth above invert elev. = 0.784 (Ft.)
 Average velocity of channel(s) = 8.639 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.774 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=K CIA) is C = 0.769
 Subarea runoff = 35.205 (CFS) for 20.500 (Ac.)
 Total runoff = 109.621 (CFS)
 Effective area this stream = 51.38 (Ac.)
 Total Study Area (Main Stream No. 1) = 79.96 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 0.862 (Ft.), Average velocity = 9.112 (Ft/s)

++++
 Process from Point/Station 130.000 to Point/Station 131.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 970.000 (Ft.)
 Top (of initial area) elevation = 957.000 (Ft.)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Bottom (of initial area) elevation = 857.000(Ft.)
 Difference in elevation = 100.000(Ft.)
 Slope = 0.10309 s(%) = 10.31
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.949 min.
 Rainfall intensity = 3.011(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.779
 Subarea runoff = 8.754(CFS)
 Total initial stream area = 3.730(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 140.000 to Point/Station 141.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm) = 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000(Ft.)
 Top (of initial area) elevation = 1103.000(Ft.)
 Bottom (of initial area) elevation = 888.000(Ft.)
 Difference in elevation = 215.000(Ft.)
 Slope = 0.21500 s(%) = 21.50
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.315 min.
 Rainfall intensity = 3.265(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.789
 Subarea runoff = 18.155(CFS)
 Total initial stream area = 7.050(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 141.000 to Point/Station 142.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.623(Ft.), Average velocity = 8.846(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	20.00	0.00
3	25.00	0.00
4	50.00	5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 42.996(CFS)
 ' ' flow top width = 10.606(Ft.)
 ' ' velocity = 8.846(Ft/s)
 ' ' area = 4.861(Sq.Ft)
 ' ' Froude number = 2.303

Upstream point elevation = 888.000(Ft.)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Downstream point elevation = 853.000(Ft.)
 Flow length = 280.000(Ft.)
 Travel time = 0.53 min.
 Time of concentration = 11.84 min.
 Depth of flow = 0.623(Ft.)
 Average velocity = 8.846(Ft/s)
 Total irregular channel flow = 42.995(CFS)
 Irregular channel normal depth above invert elev. = 0.623(Ft.)
 Average velocity of channel(s) = 8.846(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.177(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.786
 Subarea runoff = 49.611(CFS) for 20.100(Ac.)
 Total runoff = 67.766(CFS)
 Effective area this stream = 27.15(Ac.)
 Total Study Area (Main Stream No. 1) = 110.84(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.788(Ft.), Average velocity = 10.064(Ft/s)

++++++
 Process from Point/Station 150.000 to Point/Station 151.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 715.000(Ft.)
 Top (of initial area) elevation = 1066.000(Ft.)
 Bottom (of initial area) elevation = 909.000(Ft.)
 Difference in elevation = 157.000(Ft.)
 Slope = 0.21958 s(%)= 21.96
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 9.853 min.
 Rainfall intensity = 3.548(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.798
 Subarea runoff = 11.800(CFS)
 Total initial stream area = 4.170(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 151.000 to Point/Station 152.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.683(Ft.), Average velocity = 6.437(Ft/s)
 ***** Irregular Channel Data *****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 4.00
 2 15.00 0.00
 3 20.00 0.00
 4 25.00 4.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 29.487(CFS)
 ' ' flow top width = 8.415(Ft.)
 ' ' velocity= 6.437(Ft/s)
 ' ' area = 4.580(Sq.Ft)
 ' ' Froude number = 1.538

Upstream point elevation = 909.000(Ft.)
 Downstream point elevation = 863.000(Ft.)
 Flow length = 845.000(Ft.)
 Travel time = 2.19 min.
 Time of concentration = 12.04 min.
 Depth of flow = 0.683(Ft.)
 Average velocity = 6.437(Ft/s)
 Total irregular channel flow = 29.487(CFS)
 Irregular channel normal depth above invert elev. = 0.683(Ft.)
 Average velocity of channel(s) = 6.437(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.145(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.785
 Subarea runoff = 35.310(CFS) for 14.920(Ac.)
 Total runoff = 47.109(CFS)
 Effective area this stream = 19.09(Ac.)
 Total Study Area (Main Stream No. 1) = 129.93(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.883(Ft.), Average velocity = 7.407(Ft/s)

+++++
 Process from Point/Station 160.000 to Point/Station 161.000
 **** INITIAL AREA EVALUATION ****

 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 950.000(Ft.)
 Top (of initial area) elevation = 1219.000(Ft.)
 Bottom (of initial area) elevation = 991.000(Ft.)
 Difference in elevation = 228.000(Ft.)
 Slope = 0.24000 s(%)= 24.00
 TC = k(0.525)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 10.844 min.
 Rainfall intensity = 3.349(In/Hr) for a 100.0 year storm

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Effective runoff coefficient used for area (Q=KCIA) is C = 0.792
 Subarea runoff = 18.823(CFS)
 Total initial stream area = 7.100(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

+++++
 Process from Point/Station 161.000 to Point/Station 162.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.676(Ft.), Average velocity = 6.731(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	15.00	0.00
3	20.00	0.00
4	25.00	4.00

 Manning's 'N' friction factor = 0.035

Sub-Channel flow = 30.447(CFS)
 ' ' flow top width = 8.381(Ft.)
 ' ' velocity= 6.731(Ft/s)
 ' ' area = 4.523(Sq.Ft)
 ' ' Froude number = 1.615

Upstream point elevation = 991.000(Ft.)
 Downstream point elevation = 957.000(Ft.)
 Flow length = 565.000(Ft.)
 Travel time = 1.40 min.
 Time of concentration = 12.24 min.
 Depth of flow = 0.676(Ft.)
 Average velocity = 6.731(Ft/s)
 Total irregular channel flow = 30.447(CFS)
 Irregular channel normal depth above invert elev. = 0.676(Ft.)
 Average velocity of channel(s) = 6.731(Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.114(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.783
 Subarea runoff = 23.185(CFS) for 10.120(Ac.)
 Total runoff = 42.008(CFS)
 Effective area this stream = 17.22(Ac.)
 Total Study Area (Main Stream No. 1) = 147.15(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.807(Ft.), Average velocity = 7.417(Ft/s)

+++++
 Process from Point/Station 162.000 to Point/Station 163.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Depth of flow = 0.825(Ft.), Average velocity = 7.825(Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	20.00	0.00
3	25.00	0.00
4	50.00	5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 56.203(CFS)
 ' ' flow top width = 12.421(Ft.)
 ' ' velocity= 7.825(Ft/s)
 ' ' area = 7.182(Sq.Ft)
 ' ' Froude number = 1.814

Upstream point elevation = 957.000(Ft.)
 Downstream point elevation = 893.000(Ft.)
 Flow length = 890.000(Ft.)
 Travel time = 1.90 min.
 Time of concentration = 14.14 min.
 Depth of flow = 0.825(Ft.)
 Average velocity = 7.825(Ft/s)
 Total irregular channel flow = 56.203(CFS)
 Irregular channel normal depth above invert elev. = 0.825(Ft.)
 Average velocity of channel(s) = 7.825(Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 2.856(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.773
 Subarea runoff = 28.326(CFS) for 14.640(Ac.)
 Total runoff = 70.335(CFS)
 Effective area this stream = 31.86(Ac.)
 Total Study Area (Main Stream No. 1) = 161.79(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.923(Ft.), Average velocity = 8.325(Ft/s)

+++++
 Process from Point/Station 170.000 to Point/Station 171.000
 **** INITIAL AREA EVALUATION ****

 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 857.000(Ft.)
 Top (of initial area) elevation = 1138.000(Ft.)
 Bottom (of initial area) elevation = 903.000(Ft.)
 Difference in elevation = 235.000(Ft.)
 Slope = 0.27421 s(%)= 27.42

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

$TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.133 min.
 Rainfall intensity = 3.488(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.796
 Subarea runoff = 22.545(CFS)
 Total initial stream area = 8.120(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 180.000 to Point/Station 181.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Initial subarea data:
 Initial area flow distance = 996.000(Ft.)
 Top (of initial area) elevation = 1038.000(Ft.)
 Bottom (of initial area) elevation = 893.000(Ft.)
 Difference in elevation = 145.000(Ft.)
 Slope = 0.14558 s(%)= 14.56
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 12.214 min.
 Rainfall intensity = 3.119(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.784
 Subarea runoff = 21.113(CFS)
 Total initial stream area = 8.640(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 180.000 to Point/Station 181.000
 **** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Time of concentration = 12.21 min.
 Rainfall intensity = 3.119(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method)(Q=KCIA) is C = 0.784
 Subarea runoff = 28.199(CFS) for 11.540(Ac.)
 Total runoff = 49.312(CFS)
 Effective area this stream = 20.18(Ac.)
 Total Study Area (Main Stream No. 1) = 190.09(Ac.)
 Area averaged Fm value = 0.404(In/Hr)

++++++
 Process from Point/Station 200.000 to Point/Station 201.000
 **** INITIAL AREA EVALUATION ****

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 850.000 (Ft.)
 Top (of initial area) elevation = 1422.000 (Ft.)
 Bottom (of initial area) elevation = 1172.000 (Ft.)
 Difference in elevation = 250.000 (Ft.)
 Slope = 0.29412 s(%)= 29.41
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.959 min.
 Rainfall intensity = 3.525 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.797
 Subarea runoff = 19.636 (CFS)
 Total initial stream area = 6.990 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.404 (In/Hr)

++++++
 Process from Point/Station 201.000 to Point/Station 202.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 0.487 (Ft.), Average velocity = 9.323 (Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	4.00
2	15.00	0.00
3	20.00	0.00
4	30.00	4.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 29.578 (CFS)
 ' ' flow top width = 8.041 (Ft.)
 ' ' velocity= 9.323 (Ft/s)
 ' ' area = 3.173 (Sq.Ft)
 ' ' Froude number = 2.616

Upstream point elevation = 1172.000 (Ft.)
 Downstream point elevation = 1053.000 (Ft.)
 Flow length = 696.000 (Ft.)
 Travel time = 1.24 min.
 Time of concentration = 11.20 min.
 Depth of flow = 0.487 (Ft.)
 Average velocity = 9.323 (Ft/s)
 Total irregular channel flow = 29.577 (CFS)
 Irregular channel normal depth above invert elev. = 0.487 (Ft.)
 Average velocity of channel(s) = 9.323 (Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404 (In/Hr)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Rainfall intensity = 3.284(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.789
 Subarea runoff = 19.827(CFS) for 8.230(Ac.)
 Total runoff = 39.463(CFS)
 Effective area this stream = 15.22(Ac.)
 Total Study Area (Main Stream No. 1) = 205.31(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 0.571(Ft.), Average velocity = 10.193(Ft/s)

+-----+
 Process from Point/Station 202.000 to Point/Station 203.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000(CFS)
 Depth of flow = 0.863(Ft.), Average velocity = 7.971(Ft/s)
 ***** Irregular Channel Data *****

Information entered for subchannel number 1 :

Point number	'X' coordinate	'Y' coordinate
1	0.00	5.00
2	20.00	0.00
3	25.00	0.00
4	50.00	5.00

Manning's 'N' friction factor = 0.035

Sub-Channel flow = 61.154(CFS)
 ' ' flow top width = 12.771(Ft.)
 ' ' velocity = 7.971(Ft/s)
 ' ' area = 7.672(Sq.Ft)
 ' ' Froude number = 1.812

Upstream point elevation = 1053.000(Ft.)
 Downstream point elevation = 1003.000(Ft.)
 Flow length = 705.000(Ft.)
 Travel time = 1.47 min.
 Time of concentration = 12.68 min.
 Depth of flow = 0.863(Ft.)
 Average velocity = 7.971(Ft/s)
 Total irregular channel flow = 61.154(CFS)
 Irregular channel normal depth above invert elev. = 0.863(Ft.)
 Average velocity of channel(s) = 7.971(Ft/s)

Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 78.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
 Rainfall intensity = 3.050(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.781
 Subarea runoff = 43.319(CFS) for 19.540(Ac.)
 Total runoff = 82.782(CFS)
 Effective area this stream = 34.76(Ac.)
 Total Study Area (Main Stream No. 1) = 224.85(Ac.)
 Area averaged Fm value = 0.404(In/Hr)
 Depth of flow = 1.004(Ft.), Average velocity = 8.660(Ft/s)

Roquet Ranch (TTM 19982) – Drainage Report

ATTACHMENT A

Process from Point/Station 203.000 to Point/Station 204.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 1.108 (Ft.), Average velocity = 9.718 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 6.00
 2 30.00 0.00
 3 36.00 0.00
 4 60.00 6.00
 Manning's 'N' friction factor = 0.035

 Sub-Channel flow = 118.238 (CFS)
 ' ' flow top width = 15.969 (Ft.)
 ' ' velocity = 9.718 (Ft/s)
 ' ' area = 12.167 (Sq.Ft)
 ' ' Froude number = 1.962

Upstream point elevation = 1003.000 (Ft.)
 Downstream point elevation = 930.000 (Ft.)
 Flow length = 950.000 (Ft.)
 Travel time = 1.63 min.
 Time of concentration = 14.31 min.
 Depth of flow = 1.108 (Ft.)
 Average velocity = 9.718 (Ft/s)
 Total irregular channel flow = 118.237 (CFS)
 Irregular channel normal depth above invert elev. = 1.108 (Ft.)
 Average velocity of channel(s) = 9.718 (Ft/s)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 1.000
 Decimal fraction soil group C = 0.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 78.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.404 (In/Hr)
 Rainfall intensity = 2.836 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=K CIA) is C = 0.772
 Subarea runoff = 70.853 (CFS) for 35.410 (Ac.)
 Total runoff = 153.635 (CFS)
 Effective area this stream = 70.17 (Ac.)
 Total Study Area (Main Stream No. 1) = 260.26 (Ac.)
 Area averaged Fm value = 0.404 (In/Hr)
 Depth of flow = 1.261 (Ft.), Average velocity = 10.437 (Ft/s)

++++
 Process from Point/Station 204.000 to Point/Station 205.000
 **** IRREGULAR CHANNEL FLOW TRAVEL TIME ****

Estimated mean flow rate at midpoint of channel = 0.000 (CFS)
 Depth of flow = 1.678 (Ft.), Average velocity = 9.558 (Ft/s)
 ***** Irregular Channel Data *****

 Information entered for subchannel number 1 :
 Point number 'X' coordinate 'Y' coordinate
 1 0.00 7.00
 2 30.00 0.00
 3 37.00 0.00

ATTACHMENT B
Rational Method Hydrology
Proposed Condition
(10 Year & 100 Year storm)

ATTACHMENT A
Rational Method Hydrology
Proposed Condition
(10-Year storm)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2005 Version 7.1
Rational Hydrology Study Date: 02/23/16

Roquet Ranch Project - TTM 19983
Proposed Condition
10-year storm

Program License Serial Number 4029

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 10.0
Computed rainfall intensity:
Storm year = 10.00 1 hour rainfall = 0.850 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

+++++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274(In/Hr)
Initial subarea data:
Initial area flow distance = 998.000(Ft.)
Top (of initial area) elevation = 1015.600(Ft.)
Bottom (of initial area) elevation = 951.000(Ft.)
Difference in elevation = 64.600(Ft.)
Slope = 0.06473 s(%)= 6.47
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.651 min.
Rainfall intensity = 2.398(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.797
Subarea runoff = 10.897(CFS)
Total initial stream area = 5.700(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.274(In/Hr)

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 943.000(Ft.)
Downstream point/station elevation = 931.000(Ft.)
Pipe length = 900.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 10.897(CFS)
Nearest computed pipe diameter = 18.00(In.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Calculated individual pipe flow = 10.897 (CFS)
Normal flow depth in pipe = 13.34 (In.)
Flow top width inside pipe = 15.77 (In.)
Critical Depth = 15.17 (In.)
Pipe flow velocity = 7.77 (Ft/s)
Travel time through pipe = 1.93 min.
Time of concentration (TC) = 12.58 min.

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219 (In/Hr)
Time of concentration = 12.58 min.
Rainfall intensity = 2.170 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.798
Subarea runoff = 10.171 (CFS) for 6.460 (Ac.)
Total runoff = 21.069 (CFS)
Effective area this stream = 12.16 (Ac.)
Total Study Area (Main Stream No. 1) = 12.16 (Ac.)
Area averaged Fm value = 0.245 (In/Hr)

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 931.000 (Ft.)
Downstream point/station elevation = 915.000 (Ft.)
Pipe length = 1010.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 21.069 (CFS)
Nearest computed pipe diameter = 24.00 (In.)
Calculated individual pipe flow = 21.069 (CFS)
Normal flow depth in pipe = 15.36 (In.)
Flow top width inside pipe = 23.04 (In.)
Critical Depth = 19.73 (In.)
Pipe flow velocity = 9.92 (Ft/s)
Travel time through pipe = 1.70 min.
Time of concentration (TC) = 14.28 min.

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219 (In/Hr)
Time of concentration = 14.28 min.
Rainfall intensity = 2.011 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

rational method) (Q=KCIA) is C = 0.794
Subarea runoff = 6.974 (CFS) for 5.400 (Ac.)
Total runoff = 28.043 (CFS)
Effective area this stream = 17.56 (Ac.)
Total Study Area (Main Stream No. 1) = 17.56 (Ac.)
Area averaged Fm value = 0.237 (In/Hr)

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219 (In/Hr)
Time of concentration = 14.28 min.
Rainfall intensity = 2.011 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.796
Subarea runoff = 6.904 (CFS) for 4.280 (Ac.)
Total runoff = 34.946 (CFS)
Effective area this stream = 21.84 (Ac.)
Total Study Area (Main Stream No. 1) = 21.84 (Ac.)
Area averaged Fm value = 0.233 (In/Hr)

+++++
Process from Point/Station 103.000 to Point/Station 104.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 915.000 (Ft.)
Downstream point/station elevation = 910.000 (Ft.)
Pipe length = 440.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 34.946 (CFS)
Nearest computed pipe diameter = 30.00 (In.)
Calculated individual pipe flow = 34.946 (CFS)
Normal flow depth in pipe = 20.30 (In.)
Flow top width inside pipe = 28.07 (In.)
Critical Depth = 24.09 (In.)
Pipe flow velocity = 9.90 (Ft/s)
Travel time through pipe = 0.74 min.
Time of concentration (TC) = 15.02 min.

+++++
Process from Point/Station 103.000 to Point/Station 104.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219 (In/Hr)
Time of concentration = 15.02 min.
Rainfall intensity = 1.951 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.793

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Subarea runoff = 4.804(CFS) for 3.840(Ac.)
Total runoff = 39.750(CFS)
Effective area this stream = 25.68(Ac.)
Total Study Area (Main Stream No. 1) = 25.68(Ac.)
Area averaged Fm value = 0.231(In/Hr)

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 910.000(Ft.)
Downstream point/station elevation = 905.000(Ft.)
Pipe length = 100.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 39.750(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 39.750(CFS)
Normal flow depth in pipe = 16.03(In.)
Flow top width inside pipe = 22.61(In.)
Critical depth could not be calculated.
Pipe flow velocity = 17.83(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 15.11 min.

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** SUBAREA FLOW ADDITION ****

PARK subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.8500 Max loss rate(Fm)= 0.466(In/Hr)
Time of concentration = 15.11 min.
Rainfall intensity = 1.944(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.789
Subarea runoff = 1.269(CFS) for 1.080(Ac.)
Total runoff = 41.019(CFS)
Effective area this stream = 26.76(Ac.)
Total Study Area (Main Stream No. 1) = 26.76(Ac.)
Area averaged Fm value = 0.241(In/Hr)

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 26.760(Ac.)
Runoff from this stream = 41.019(CFS)
Time of concentration = 15.11 min.
Rainfall intensity = 1.944(In/Hr)
Area averaged loss rate (Fm) = 0.2408(In/Hr)
Area averaged Pervious ratio (Ap) = 0.4395

++++
Process from Point/Station 106.000 to Point/Station 107.000
**** INITIAL AREA EVALUATION ****

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274(In/Hr)
 Initial subarea data:
 Initial area flow distance = 855.000(Ft.)
 Top (of initial area) elevation = 998.000(Ft.)
 Bottom (of initial area) elevation = 962.000(Ft.)
 Difference in elevation = 36.000(Ft.)
 Slope = 0.04211 s(%)= 4.21
 $TC = k(0.389)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 10.911 min.
 Rainfall intensity = 2.364(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.796
 Subarea runoff = 8.407(CFS)
 Total initial stream area = 4.470(Ac.)
 Pervious area fraction = 0.500
 Initial area Fm value = 0.274(In/Hr)

 Process from Point/Station 107.000 to Point/Station 105.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 955.000(Ft.)
 Downstream point/station elevation = 905.000(Ft.)
 Pipe length = 950.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 8.407(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 8.407(CFS)
 Normal flow depth in pipe = 8.09(In.)
 Flow top width inside pipe = 14.95(In.)
 Critical Depth = 13.59(In.)
 Pipe flow velocity = 12.45(Ft/s)
 Travel time through pipe = 1.27 min.
 Time of concentration (TC) = 12.18 min.

 Process from Point/Station 107.000 to Point/Station 105.000
 **** SUBAREA FLOW ADDITION ****

RESIDENTIAL(5 - 7 dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274(In/Hr)
 Time of concentration = 12.18 min.
 Rainfall intensity = 2.212(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.789
 Subarea runoff = 6.858(CFS) for 4.280(Ac.)
 Total runoff = 15.265(CFS)
 Effective area this stream = 8.75(Ac.)
 Total Study Area (Main Stream No. 1) = 35.51(Ac.)
 Area averaged Fm value = 0.274(In/Hr)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

+++++
Process from Point/Station 107.000 to Point/Station 105.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 8.750 (Ac.)
Runoff from this stream = 15.265 (CFS)
Time of concentration = 12.18 min.
Rainfall intensity = 2.212 (In/Hr)
Area averaged loss rate (Fm) = 0.2740 (In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000

+++++
Process from Point/Station 108.000 to Point/Station 109.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 69.00
Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.055 (In/Hr)
Initial subarea data:
Initial area flow distance = 525.000 (Ft.)
Top (of initial area) elevation = 994.400 (Ft.)
Bottom (of initial area) elevation = 932.000 (Ft.)
Difference in elevation = 62.400 (Ft.)
Slope = 0.11886 s(%) = 11.89
TC = $k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
Initial area time of concentration = 5.701 min.
Rainfall intensity = 3.489 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.886
Subarea runoff = 3.555 (CFS)
Total initial stream area = 1.150 (Ac.)
Pervious area fraction = 0.100
Initial area Fm value = 0.055 (In/Hr)

+++++
Process from Point/Station 109.000 to Point/Station 110.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 932.000 (Ft.)
End of street segment elevation = 916.800 (Ft.)
Length of street segment = 610.000 (Ft.)
Height of curb above gutter flowline = 6.0 (In.)
Width of half street (curb to crown) = 16.500 (Ft.)
Distance from crown to crossfall grade break = 2.000 (Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line = 13.500 (Ft.)
Slope from curb to property line (v/hz) = 0.025
Gutter width = 2.000 (Ft.)
Gutter hike from flowline = 2.000 (In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150
Estimated mean flow rate at midpoint of street = 5.356 (CFS)
Depth of flow = 0.353 (Ft.), Average velocity = 3.813 (Ft/s)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 11.305(Ft.)
 Flow velocity = 3.81(Ft/s)
 Travel time = 2.67 min. TC = 8.37 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Rainfall intensity = 2.772(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.882
 Subarea runoff = 3.537(CFS) for 1.750(Ac.)
 Total runoff = 7.091(CFS)
 Effective area this stream = 2.90(Ac.)
 Total Study Area (Main Stream No. 1) = 38.41(Ac.)
 Area averaged Fm value = 0.055(In/Hr)
 Street flow at end of street = 7.091(CFS)
 Half street flow at end of street = 7.091(CFS)
 Depth of flow = 0.381(Ft.), Average velocity = 4.073(Ft/s)
 Flow width (from curb towards crown)= 12.705(Ft.)

+++++
 Process from Point/Station 110.000 to Point/Station 105.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 909.000(Ft.)
 Downstream point/station elevation = 905.000(Ft.)
 Pipe length = 100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 7.091(CFS)
 Nearest computed pipe diameter = 12.00(In.)
 Calculated individual pipe flow = 7.091(CFS)
 Normal flow depth in pipe = 9.77(In.)
 Flow top width inside pipe = 9.33(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 10.34(Ft/s)
 Travel time through pipe = 0.16 min.
 Time of concentration (TC) = 8.53 min.

+++++
 Process from Point/Station 110.000 to Point/Station 105.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 2.900(Ac.)
 Runoff from this stream = 7.091(CFS)
 Time of concentration = 8.53 min.
 Rainfall intensity = 2.740(In/Hr)
 Area averaged loss rate (Fm) = 0.0548(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
1	41.02	26.760	15.11	0.241	1.944
2	15.27	8.750	12.18	0.274	2.212

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

3	7.09	2.900	8.53	0.055	2.740
Qmax(1) =					
	1.000 *	1.000 *	41.019)	+	
	0.862 *	1.000 *	15.265)	+	
	0.703 *	1.000 *	7.091)	+	= 59.159
Qmax(2) =					
	1.158 *	0.806 *	41.019)	+	
	1.000 *	1.000 *	15.265)	+	
	0.803 *	1.000 *	7.091)	+	= 59.239
Qmax(3) =					
	1.468 *	0.564 *	41.019)	+	
	1.272 *	0.700 *	15.265)	+	
	1.000 *	1.000 *	7.091)	+	= 54.656

Total of 3 streams to confluence:
Flow rates before confluence point:
41.019 15.265 7.091
Maximum flow rates at confluence using above data:
59.159 59.239 54.656
Area of streams before confluence:
26.760 8.750 2.900
Effective area values after confluence:
38.410 33.220 24.125

Results of confluence:
Total flow rate = 59.239(CFS)
Time of concentration = 12.182 min.
Effective stream area after confluence = 33.220(Ac.)
Study area average Pervious fraction(Ap) = 0.428
Study area average soil loss rate(Fm) = 0.234(In/Hr)
Study area total (this main stream) = 38.41(Ac.)

+++++
Process from Point/Station 105.000 to Point/Station 111.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 905.000(Ft.)
Downstream point/station elevation = 904.000(Ft.)
Pipe length = 60.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 59.239(CFS)
Nearest computed pipe diameter = 33.00(In.)
Calculated individual pipe flow = 59.239(CFS)
Normal flow depth in pipe = 23.77(In.)
Flow top width inside pipe = 29.63(In.)
Critical Depth = 29.73(In.)
Pipe flow velocity = 12.95(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 12.26 min.

+++++
Process from Point/Station 105.000 to Point/Station 111.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 33.220(Ac.)
Runoff from this stream = 59.239(CFS)
Time of concentration = 12.26 min.
Rainfall intensity = 2.204(In/Hr)
Area averaged loss rate (Fm) = 0.2343(In/Hr)
Area averaged Pervious ratio (Ap) = 0.4276

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Process from Point/Station 112.000 to Point/Station 113.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Initial subarea data:
 Initial area flow distance = 990.000(Ft.)
 Top (of initial area) elevation = 1100.000(Ft.)
 Bottom (of initial area) elevation = 925.000(Ft.)
 Difference in elevation = 175.000(Ft.)
 Slope = 0.17677 s(%)= 17.68
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.720 min.
 Rainfall intensity = 2.264(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.795
 Subarea runoff = 13.675(CFS)
 Total initial stream area = 7.600(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265(In/Hr)

Process from Point/Station 113.000 to Point/Station 111.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 918.000(Ft.)
 Downstream point/station elevation = 904.000(Ft.)
 Pipe length = 150.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 13.675(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 13.675(CFS)
 Normal flow depth in pipe = 9.19(In.)
 Flow top width inside pipe = 14.62(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 17.36(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 11.86 min.

Process from Point/Station 113.000 to Point/Station 111.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 7.600(Ac.)
 Runoff from this stream = 13.675(CFS)
 Time of concentration = 11.86 min.
 Rainfall intensity = 2.248(In/Hr)
 Area averaged loss rate (Fm) = 0.2651(In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
1	59.24	33.220	12.26	0.234	2.204

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

2	13.68	7.600	11.86	0.265	2.248
Qmax(1) =					
	1.000 *	1.000 *	59.239)	+	
	0.978 *	1.000 *	13.675)	+	72.612
Qmax(2) =					
	1.022 *	0.968 *	59.239)	+	
	1.000 *	1.000 *	13.675)	+	72.277

Total of 2 streams to confluence:
Flow rates before confluence point:
59.239 13.675
Maximum flow rates at confluence using above data:
72.612 72.277
Area of streams before confluence:
33.220 7.600
Effective area values after confluence:
40.820 39.748
Results of confluence:
Total flow rate = 72.612(CFS)
Time of concentration = 12.260 min.
Effective stream area after confluence = 40.820(Ac.)
Study area average Pervious fraction(Ap) = 0.534
Study area average soil loss rate(Fm) = 0.240(In/Hr)
Study area total (this main stream) = 40.82(Ac.)

+++++
Process from Point/Station 111.000 to Point/Station 120.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 904.000(Ft.)
Downstream point/station elevation = 899.000(Ft.)
Pipe length = 715.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 72.612(CFS)
Nearest computed pipe diameter = 42.00(In.)
Calculated individual pipe flow = 72.612(CFS)
Normal flow depth in pipe = 30.09(In.)
Flow top width inside pipe = 37.86(In.)
Critical Depth = 32.02(In.)
Pipe flow velocity = 9.84(Ft/s)
Travel time through pipe = 1.21 min.
Time of concentration (TC) = 13.47 min.

+++++
Process from Point/Station 111.000 to Point/Station 120.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 40.820(Ac.)
Runoff from this stream = 72.612(CFS)
Time of concentration = 13.47 min.
Rainfall intensity = 2.083(In/Hr)
Area averaged loss rate (Fm) = 0.2400(In/Hr)
Area averaged Pervious ratio (Ap) = 0.5342

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274(In/Hr)
Initial subarea data:
Initial area flow distance = 795.000(Ft.)
Top (of initial area) elevation = 1075.000(Ft.)
Bottom (of initial area) elevation = 1058.000(Ft.)
Difference in elevation = 17.000(Ft.)
Slope = 0.02138 s(%)= 2.14
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 12.136 min.
Rainfall intensity = 2.217(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.789
Subarea runoff = 7.801(CFS)
Total initial stream area = 4.460(Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.274(In/Hr)

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 12.14 min.
Rainfall intensity = 2.217(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.802
Subarea runoff = 12.518(CFS) for 6.960(Ac.)
Total runoff = 20.319(CFS)
Effective area this stream = 11.42(Ac.)
Total Study Area (Main Stream No. 1) = 57.43(Ac.)
Area averaged Fm value = 0.241(In/Hr)

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 12.14 min.
Rainfall intensity = 2.217(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.812
Subarea runoff = 3.095(CFS) for 1.590(Ac.)
Total runoff = 23.414(CFS)
Effective area this stream = 13.01(Ac.)
Total Study Area (Main Stream No. 1) = 59.02(Ac.)
Area averaged Fm value = 0.218(In/Hr)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

+++++
Process from Point/Station 122.000 to Point/Station 123.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1050.000(Ft.)
Downstream point/station elevation = 980.000(Ft.)
Pipe length = 1850.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 23.414(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 23.414(CFS)
Normal flow depth in pipe = 13.69(In.)
Flow top width inside pipe = 20.01(In.)
Critical Depth = 19.93(In.)
Pipe flow velocity = 14.10(Ft/s)
Travel time through pipe = 2.19 min.
Time of concentration (TC) = 14.32 min.

+++++
Process from Point/Station 122.000 to Point/Station 123.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274(In/Hr)
Time of concentration = 14.32 min.
Rainfall intensity = 2.008(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.793
Subarea runoff = 8.824(CFS) for 7.230(Ac.)
Total runoff = 32.238(CFS)
Effective area this stream = 20.24(Ac.)
Total Study Area (Main Stream No. 1) = 66.25(Ac.)
Area averaged Fm value = 0.238(In/Hr)

+++++
Process from Point/Station 123.000 to Point/Station 124.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 980.000(Ft.)
Downstream point/station elevation = 932.000(Ft.)
Pipe length = 785.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 32.238(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 32.238(CFS)
Normal flow depth in pipe = 14.51(In.)
Flow top width inside pipe = 19.41(In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.19(Ft/s)
Travel time through pipe = 0.72 min.
Time of concentration (TC) = 15.04 min.

+++++
Process from Point/Station 123.000 to Point/Station 124.000
**** SUBAREA FLOW ADDITION ****

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 15.04 min.
Rainfall intensity = 1.949(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.791
Subarea runoff = 3.052(CFS) for 2.640(Ac.)
Total runoff = 35.289(CFS)
Effective area this stream = 22.88(Ac.)
Total Study Area (Main Stream No. 1) = 68.89(Ac.)
Area averaged Fm value = 0.236(In/Hr)

+++++
Process from Point/Station 123.000 to Point/Station 124.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 15.04 min.
Rainfall intensity = 1.949(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.789
Subarea runoff = 5.412(CFS) for 3.570(Ac.)
Total runoff = 40.701(CFS)
Effective area this stream = 26.45(Ac.)
Total Study Area (Main Stream No. 1) = 72.46(Ac.)
Area averaged Fm value = 0.240(In/Hr)

+++++
Process from Point/Station 124.000 to Point/Station 120.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 932.000(Ft.)
Downstream point/station elevation = 898.000(Ft.)
Pipe length = 1070.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 40.701(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 40.701(CFS)
Normal flow depth in pipe = 17.25(In.)
Flow top width inside pipe = 25.94(In.)
Critical Depth = 25.21(In.)
Pipe flow velocity = 15.19(Ft/s)
Travel time through pipe = 1.17 min.
Time of concentration (TC) = 16.22 min.

+++++
Process from Point/Station 124.000 to Point/Station 120.000
**** CONFLUENCE OF MINOR STREAMS ****

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 26.450 (Ac.)
 Runoff from this stream = 40.701 (CFS)
 Time of concentration = 16.22 min.
 Rainfall intensity = 1.864 (In/Hr)
 Area averaged loss rate (Fm) = 0.2397 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5071
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
------------	-----------------	------------	----------	------------	----------------------------

1	72.61	40.820	13.47	0.240	2.083
2	40.70	26.450	16.22	0.240	1.864

Qmax(1) =
 1.000 * 1.000 * 72.612) +
 1.135 * 0.831 * 40.701) + = 110.989
 Qmax(2) =
 0.881 * 1.000 * 72.612) +
 1.000 * 1.000 * 40.701) + = 104.668

Total of 2 streams to confluence:
 Flow rates before confluence point:
 72.612 40.701
 Maximum flow rates at confluence using above data:
 110.989 104.668
 Area of streams before confluence:
 40.820 26.450
 Effective area values after confluence:
 62.792 67.270

Results of confluence:
 Total flow rate = 110.989 (CFS)
 Time of concentration = 13.471 min.
 Effective stream area after confluence = 62.792 (Ac.)
 Study area average Pervious fraction (Ap) = 0.524
 Study area average soil loss rate (Fm) = 0.240 (In/Hr)
 Study area total (this main stream) = 67.27 (Ac.)

++++++
 Process from Point/Station 200.000 to Point/Station 201.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL(11+ dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio (Ap) = 0.2000 Max loss rate (Fm) = 0.110 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 825.000 (Ft.)
 Top (of initial area) elevation = 914.700 (Ft.)
 Bottom (of initial area) elevation = 910.300 (Ft.)
 Difference in elevation = 4.400 (Ft.)
 Slope = 0.00533 s(%) = 0.53
 TC = k(0.324)*[(length^3)/(elevation change)]^0.2
 Initial area time of concentration = 13.543 min.
 Rainfall intensity = 2.076 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.852
 Subarea runoff = 8.637 (CFS)
 Total initial stream area = 4.880 (Ac.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Pervious area fraction = 0.200
Initial area Fm value = 0.110(In/Hr)

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 903.000(Ft.)
Downstream point/station elevation = 899.000(Ft.)
Pipe length = 506.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 8.637(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 8.637(CFS)
Normal flow depth in pipe = 13.66(In.)
Flow top width inside pipe = 15.39(In.)
Critical Depth = 13.65(In.)
Pipe flow velocity = 6.00(Ft/s)
Travel time through pipe = 1.41 min.
Time of concentration (TC) = 14.95 min.

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(11+ dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
Time of concentration = 14.95 min.
Rainfall intensity = 1.957(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.850
Subarea runoff = 9.484(CFS) for 6.020(Ac.)
Total runoff = 18.121(CFS)
Effective area this stream = 10.90(Ac.)
Total Study Area (Main Stream No. 1) = 83.36(Ac.)
Area averaged Fm value = 0.110(In/Hr)

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(11+ dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
Time of concentration = 14.95 min.
Rainfall intensity = 1.957(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.850
Subarea runoff = 16.957(CFS) for 10.200(Ac.)
Total runoff = 35.078(CFS)
Effective area this stream = 21.10(Ac.)
Total Study Area (Main Stream No. 1) = 93.56(Ac.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Area averaged Fm value = 0.110 (In/Hr)

+++++
Process from Point/Station 202.000 to Point/Station 203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 899.000 (Ft.)
Downstream point/station elevation = 857.000 (Ft.)
Pipe length = 675.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 35.078 (CFS)
Nearest computed pipe diameter = 21.00 (In.)
Calculated individual pipe flow = 35.078 (CFS)
Normal flow depth in pipe = 15.40 (In.)
Flow top width inside pipe = 18.57 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.56 (Ft/s)
Travel time through pipe = 0.61 min.
Time of concentration (TC) = 15.56 min.

+++++
Process from Point/Station 202.000 to Point/Station 203.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 86.00
Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.265 (In/Hr)
Time of concentration = 15.56 min.
Rainfall intensity = 1.911 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.841
Subarea runoff = 2.605 (CFS) for 2.350 (Ac.)
Total runoff = 37.683 (CFS)
Effective area this stream = 23.45 (Ac.)
Total Study Area (Main Stream No. 1) = 95.91 (Ac.)
Area averaged Fm value = 0.125 (In/Hr)

+++++
Process from Point/Station 300.000 to Point/Station 301.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 69.00
Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.055 (In/Hr)
Initial subarea data:
Initial area flow distance = 1000.000 (Ft.)
Top (of initial area) elevation = 920.000 (Ft.)
Bottom (of initial area) elevation = 857.000 (Ft.)
Difference in elevation = 63.000 (Ft.)
Slope = 0.06300 s(%) = 6.30
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.375 min.
Rainfall intensity = 2.770 (In/Hr) for a 10.0 year storm

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Effective runoff coefficient used for area (Q=KCIA) is C = 0.882
Subarea runoff = 7.649(CFS)
Total initial stream area = 3.130(Ac.)
Pervious area fraction = 0.100
Initial area Fm value = 0.055(In/Hr)

+++++
Process from Point/Station 301.000 to Point/Station 302.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 851.000(Ft.)
Downstream point/station elevation = 846.000(Ft.)
Pipe length = 1250.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 7.649(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 7.649(CFS)
Normal flow depth in pipe = 13.73(In.)
Flow top width inside pipe = 19.98(In.)
Critical Depth = 12.29(In.)
Pipe flow velocity = 4.59(Ft/s)
Travel time through pipe = 4.54 min.
Time of concentration (TC) = 12.92 min.

+++++
Process from Point/Station 301.000 to Point/Station 302.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 12.92 min.
Rainfall intensity = 2.136(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.877
Subarea runoff = 5.238(CFS) for 3.750(Ac.)
Total runoff = 12.888(CFS)
Effective area this stream = 6.88(Ac.)
Total Study Area (Main Stream No. 1) = 102.79(Ac.)
Area averaged Fm value = 0.055(In/Hr)

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 846.000(Ft.)
Downstream point/station elevation = 842.000(Ft.)
Pipe length = 60.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 12.888(CFS)
Nearest computed pipe diameter = 15.00(In.)
Calculated individual pipe flow = 12.888(CFS)
Normal flow depth in pipe = 9.89(In.)
Flow top width inside pipe = 14.22(In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.00(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 12.98 min.

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

```

+++++
Process from Point/Station      302.000 to Point/Station      303.000
**** SUBAREA FLOW ADDITION ****

```

```

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000      Max loss rate(Fm)=      0.265(In/Hr)
Time of concentration =      12.98 min.
Rainfall intensity =      2.130(In/Hr) for a      10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.871
Subarea runoff =      0.731(CFS) for      0.460(Ac.)
Total runoff =      13.619(CFS)
Effective area this stream =      7.34(Ac.)
Total Study Area (Main Stream No. 1) =      103.25(Ac.)
Area averaged Fm value =      0.068(In/Hr)

```

```

+++++
Process from Point/Station      400.000 to Point/Station      401.000
**** INITIAL AREA EVALUATION ****

```

```

APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000      Max loss rate(Fm)=      0.110(In/Hr)
Initial subarea data:
Initial area flow distance =      615.000(Ft.)
Top (of initial area) elevation =      862.000(Ft.)
Bottom (of initial area) elevation =      852.000(Ft.)
Difference in elevation =      10.000(Ft.)
Slope =      0.01626 s(%)=      1.63
TC = k(0.324)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =      9.635 min.
Rainfall intensity =      2.547(In/Hr) for a      10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.861
Subarea runoff =      4.913(CFS)
Total initial stream area =      2.240(Ac.)
Pervious area fraction = 0.200
Initial area Fm value =      0.110(In/Hr)

```

```

+++++
Process from Point/Station      500.000 to Point/Station      501.000
**** INITIAL AREA EVALUATION ****

```

```

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000      Max loss rate(Fm)=      0.265(In/Hr)
Initial subarea data:

```

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Initial area flow distance = 847.000 (Ft.)
 Top (of initial area) elevation = 1393.600 (Ft.)
 Bottom (of initial area) elevation = 1044.000 (Ft.)
 Difference in elevation = 349.600 (Ft.)
 Slope = 0.41275 s(%) = 41.28
 $TC = k(0.525) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.293 min.
 Rainfall intensity = 2.603 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.808
 Subarea runoff = 11.045 (CFS)
 Total initial stream area = 5.250 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265 (In/Hr)

++++++
 Process from Point/Station 501.000 to Point/Station 502.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1044.000 (Ft.)
 Downstream point elevation = 995.000 (Ft.)
 Channel length thru subarea = 895.000 (Ft.)
 Channel base width = 2.000 (Ft.)
 Slope or 'Z' of left channel bank = 2.000
 Slope or 'Z' of right channel bank = 2.000
 Estimated mean flow rate at midpoint of channel = 22.099 (CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 3.000 (Ft.)
 Flow (q) thru subarea = 22.099 (CFS)
 Depth of flow = 0.568 (Ft.), Average velocity = 12.418 (Ft/s)
 Channel flow top width = 4.270 (Ft.)
 Flow Velocity = 12.42 (Ft/s)
 Travel time = 1.20 min.
 Time of concentration = 10.49 min.
 Critical depth = 1.094 (Ft.)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 86.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.265 (In/Hr)
 Rainfall intensity = 2.420 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.801
 Subarea runoff = 22.015 (CFS) for 11.800 (Ac.)
 Total runoff = 33.060 (CFS)
 Effective area this stream = 17.05 (Ac.)
 Total Study Area (Main Stream No. 1) = 122.54 (Ac.)
 Area averaged Fm value = 0.265 (In/Hr)
 Depth of flow = 0.700 (Ft.), Average velocity = 13.891 (Ft/s)
 Critical depth = 1.344 (Ft.)

++++++
 Process from Point/Station 502.000 to Point/Station 503.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 995.000 (Ft.)
 Downstream point elevation = 984.000 (Ft.)
 Channel length thru subarea = 505.000 (Ft.)
 Channel base width = 2.000 (Ft.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 0.000
Estimated mean flow rate at midpoint of channel = 35.844 (CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000 (Ft.)
Flow(q) thru subarea = 35.844 (CFS)
Depth of flow = 1.098 (Ft.), Average velocity = 10.544 (Ft/s)
Channel flow top width = 4.195 (Ft.)
Flow Velocity = 10.54 (Ft/s)
Travel time = 0.80 min.
Time of concentration = 11.29 min.
Critical depth = 1.641 (Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
Rainfall intensity = 2.315 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.797
Subarea runoff = 5.507 (CFS) for 3.850 (Ac.)
Total runoff = 38.566 (CFS)
Effective area this stream = 20.90 (Ac.)
Total Study Area (Main Stream No. 1) = 126.39 (Ac.)
Area averaged Fm value = 0.265 (In/Hr)
Depth of flow = 1.142 (Ft.), Average velocity = 10.746 (Ft/s)
Critical depth = 1.703 (Ft.)

+++++
Process from Point/Station 503.000 to Point/Station 504.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 984.000 (Ft.)
Downstream point elevation = 939.000 (Ft.)
Channel length thru subarea = 688.000 (Ft.)
Channel base width = 2.000 (Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 43.008 (CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000 (Ft.)
Flow(q) thru subarea = 43.008 (CFS)
Depth of flow = 0.765 (Ft.), Average velocity = 15.922 (Ft/s)
Channel flow top width = 5.061 (Ft.)
Flow Velocity = 15.92 (Ft/s)
Travel time = 0.72 min.
Time of concentration = 12.01 min.
Critical depth = 1.531 (Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
Rainfall intensity = 2.231 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.793

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Subarea runoff = 8.818(CFS) for 5.880(Ac.)
Total runoff = 47.384(CFS)
Effective area this stream = 26.78(Ac.)
Total Study Area (Main Stream No. 1) = 132.27(Ac.)
Area averaged Fm value = 0.265(In/Hr)
Depth of flow = 0.804(Ft.), Average velocity = 16.346(Ft/s)
Critical depth = 1.609(Ft.)

+++++
Process from Point/Station 504.000 to Point/Station 505.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 939.000(Ft.)
Downstream point elevation = 905.000(Ft.)
Channel length thru subarea = 1140.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 48.689(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 48.689(CFS)
Depth of flow = 0.990(Ft.), Average velocity = 12.349(Ft/s)
Channel flow top width = 5.962(Ft.)
Flow Velocity = 12.35(Ft/s)
Travel time = 1.54 min.
Time of concentration = 13.55 min.
Critical depth = 1.625(Ft.)

Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 2.075(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.785
Subarea runoff = 2.538(CFS) for 3.860(Ac.)
Total runoff = 49.923(CFS)
Effective area this stream = 30.64(Ac.)
Total Study Area (Main Stream No. 1) = 136.13(Ac.)
Area averaged Fm value = 0.265(In/Hr)
Depth of flow = 1.003(Ft.), Average velocity = 12.431(Ft/s)
Critical depth = 1.641(Ft.)

+++++
Process from Point/Station 504.000 to Point/Station 505.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 13.55 min.
Rainfall intensity = 2.075(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

rational method) (Q=KCIA) is C = 0.785
 Subarea runoff = 6.273(CFS) for 3.850(Ac.)
 Total runoff = 56.196(CFS)
 Effective area this stream = 34.49(Ac.)
 Total Study Area (Main Stream No. 1) = 139.98(Ac.)
 Area averaged Fm value = 0.265(In/Hr)

+++++
 Process from Point/Station 600.000 to Point/Station 601.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Initial subarea data:
 Initial area flow distance = 865.000(Ft.)
 Top (of initial area) elevation = 994.400(Ft.)
 Bottom (of initial area) elevation = 913.600(Ft.)
 Difference in elevation = 80.800(Ft.)
 Slope = 0.09341 s(%)= 9.34
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 7.305 min.
 Rainfall intensity = 3.007(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.884
 Subarea runoff = 11.638(CFS)
 Total initial stream area = 4.380(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.055(In/Hr)

+++++
 Process from Point/Station 600.000 to Point/Station 601.000
 **** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Time of concentration = 7.30 min.
 Rainfall intensity = 3.007(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.884
 Subarea runoff = 12.063(CFS) for 4.540(Ac.)
 Total runoff = 23.701(CFS)
 Effective area this stream = 8.92(Ac.)
 Total Study Area (Main Stream No. 1) = 148.90(Ac.)
 Area averaged Fm value = 0.055(In/Hr)

+++++
 Process from Point/Station 601.000 to Point/Station 602.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 908.000(Ft.)
 Downstream point/station elevation = 885.000(Ft.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Pipe length = 300.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 23.701(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 23.701(CFS)
Normal flow depth in pipe = 12.35(In.)
Flow top width inside pipe = 16.71(In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.35(Ft/s)
Travel time through pipe = 0.27 min.
Time of concentration (TC) = 7.58 min.

+++++
Process from Point/Station 601.000 to Point/Station 602.000
**** SUBAREA FLOW ADDITION ****

APARTMENT subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
Time of concentration = 7.58 min.
Rainfall intensity = 2.942(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.874
Subarea runoff = 25.475(CFS) for 10.200(Ac.)
Total runoff = 49.176(CFS)
Effective area this stream = 19.12(Ac.)
Total Study Area (Main Stream No. 1) = 159.10(Ac.)
Area averaged Fm value = 0.084(In/Hr)

+++++
Process from Point/Station 602.000 to Point/Station 603.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 885.000(Ft.)
Downstream point/station elevation = 882.000(Ft.)
Pipe length = 80.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 49.176(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 49.176(CFS)
Normal flow depth in pipe = 18.61(In.)
Flow top width inside pipe = 24.99(In.)
Critical depth could not be calculated.
Pipe flow velocity = 16.83(Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 7.66 min.

+++++
Process from Point/Station 602.000 to Point/Station 603.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Time of concentration = 7.66 min.
Rainfall intensity = 2.923(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.871
Subarea runoff = 2.771(CFS) for 1.290(Ac.)
Total runoff = 51.947(CFS)
Effective area this stream = 20.41(Ac.)
Total Study Area (Main Stream No. 1) = 160.39(Ac.)
Area averaged Fm value = 0.095(In/Hr)

+++++
Process from Point/Station 700.000 to Point/Station 701.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Initial subarea data:
Initial area flow distance = 998.000(Ft.)
Top (of initial area) elevation = 1477.000(Ft.)
Bottom (of initial area) elevation = 1082.000(Ft.)
Difference in elevation = 395.000(Ft.)
Slope = 0.39579 s(%)= 39.58
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.007 min.
Rainfall intensity = 2.490(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.804
Subarea runoff = 10.290(CFS)
Total initial stream area = 5.140(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.265(In/Hr)

+++++
Process from Point/Station 701.000 to Point/Station 702.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1082.000(Ft.)
Downstream point elevation = 983.000(Ft.)
Channel length thru subarea = 800.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 15.064(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 15.064(CFS)
Depth of flow = 0.370(Ft.), Average velocity = 14.834(Ft/s)
Channel flow top width = 3.482(Ft.)
Flow Velocity = 14.83(Ft/s)
Travel time = 0.90 min.
Time of concentration = 10.91 min.
Critical depth = 0.898(Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Rainfall intensity = 2.364(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method) (Q=KCIA) is C = 0.799
 Subarea runoff = 9.472(CFS) for 5.320(Ac.)
 Total runoff = 19.762(CFS)
 Effective area this stream = 10.46(Ac.)
 Total Study Area (Main Stream No. 1) = 170.85(Ac.)
 Area averaged Fm value = 0.265(In/Hr)
 Depth of flow = 0.430(Ft.), Average velocity = 16.078(Ft/s)
 Critical depth = 1.031(Ft.)

++++++
 Process from Point/Station 701.000 to Point/Station 702.000
 **** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Time of concentration = 10.91 min.
 Rainfall intensity = 2.364(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method) (Q=KCIA) is C = 0.806
 Subarea runoff = 2.079(CFS) for 1.000(Ac.)
 Total runoff = 21.841(CFS)
 Effective area this stream = 11.46(Ac.)
 Total Study Area (Main Stream No. 1) = 171.85(Ac.)
 Area averaged Fm value = 0.247(In/Hr)

++++++
 Process from Point/Station 701.000 to Point/Station 702.000
 **** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Time of concentration = 10.91 min.
 Rainfall intensity = 2.364(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method) (Q=KCIA) is C = 0.801
 Subarea runoff = 48.366(CFS) for 25.600(Ac.)
 Total runoff = 70.207(CFS)
 Effective area this stream = 37.06(Ac.)
 Total Study Area (Main Stream No. 1) = 197.45(Ac.)
 Area averaged Fm value = 0.259(In/Hr)

++++++
 Process from Point/Station 702.000 to Point/Station 703.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Upstream point elevation = 983.000 (Ft.)
Downstream point elevation = 973.000 (Ft.)
Channel length thru subarea = 435.000 (Ft.)
Channel base width = 2.000 (Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 85.328 (CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000 (Ft.)
Flow (q) thru subarea = 85.328 (CFS)
Depth of flow = 1.380 (Ft.), Average velocity = 12.987 (Ft/s)
Channel flow top width = 7.521 (Ft.)
Flow Velocity = 12.99 (Ft/s)
Travel time = 0.56 min.
Time of concentration = 11.46 min.
Critical depth = 2.125 (Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 86.00
Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.265 (In/Hr)
Rainfall intensity = 2.295 (In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.798
Subarea runoff = 30.185 (CFS) for 17.800 (Ac.)
Total runoff = 100.392 (CFS)
Effective area this stream = 54.86 (Ac.)
Total Study Area (Main Stream No. 1) = 215.25 (Ac.)
Area averaged Fm value = 0.261 (In/Hr)
Depth of flow = 1.489 (Ft.), Average velocity = 13.542 (Ft/s)
Critical depth = 2.297 (Ft.)

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 973.000 (Ft.)
Downstream point/station elevation = 953.000 (Ft.)
Pipe length = 150.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 100.392 (CFS)
Nearest computed pipe diameter = 27.00 (In.)
Calculated individual pipe flow = 100.392 (CFS)
Normal flow depth in pipe = 19.80 (In.)
Flow top width inside pipe = 23.87 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 32.13 (Ft/s)
Travel time through pipe = 0.08 min.
Time of concentration (TC) = 11.54 min.

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 11.54 min.
Rainfall intensity = 2.285(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.797
Subarea runoff = 4.141(CFS) for 2.530(Ac.)
Total runoff = 104.533(CFS)
Effective area this stream = 57.39(Ac.)
Total Study Area (Main Stream No. 1) = 217.78(Ac.)
Area averaged Fm value = 0.261(In/Hr)

++++
Process from Point/Station 703.000 to Point/Station 704.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 11.54 min.
Rainfall intensity = 2.285(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.798
Subarea runoff = 2.007(CFS) for 1.000(Ac.)
Total runoff = 106.540(CFS)
Effective area this stream = 58.39(Ac.)
Total Study Area (Main Stream No. 1) = 218.78(Ac.)
Area averaged Fm value = 0.258(In/Hr)

++++
Process from Point/Station 703.000 to Point/Station 704.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 58.390(Ac.)
Runoff from this stream = 106.540(CFS)
Time of concentration = 11.54 min.
Rainfall intensity = 2.285(In/Hr)
Area averaged loss rate (Fm) = 0.2579(In/Hr)
Area averaged Pervious ratio (Ap) = 0.9692

++++
Process from Point/Station 705.000 to Point/Station 706.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Initial subarea data:
Initial area flow distance = 800.000(Ft.)
Top (of initial area) elevation = 1058.800(Ft.)
Bottom (of initial area) elevation = 1017.000(Ft.)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Difference in elevation = 41.800(Ft.)
 Slope = 0.05225 s(%)= 5.22
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 7.952 min.
 Rainfall intensity = 2.858(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.883
 Subarea runoff = 6.079(CFS)
 Total initial stream area = 2.410(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.055(In/Hr)

++++++
 Process from Point/Station 706.000 to Point/Station 707.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1017.000(Ft.)
 End of street segment elevation = 994.000(Ft.)
 Length of street segment = 485.000(Ft.)
 Height of curb above gutter flowline = 6.0(In.)
 Width of half street (curb to crown) = 16.500(Ft.)
 Distance from crown to crossfall grade break = 2.000(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.500(Ft.)
 Slope from curb to property line (v/hz) = 0.025
 Gutter width = 2.000(Ft.)
 Gutter hike from flowline = 2.000(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 16.061(CFS)
 Depth of flow = 0.437(Ft.), Average velocity = 6.328(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 15.528(Ft.)
 Flow velocity = 6.33(Ft/s)
 Travel time = 1.28 min. TC = 9.23 min.
 Adding area flow to street
 APARTMENT subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
 Rainfall intensity = 2.613(In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method) (Q=KCIA) is C = 0.866
 Subarea runoff = 19.863(CFS) for 9.050(Ac.)
 Total runoff = 25.943(CFS)
 Effective area this stream = 11.46(Ac.)
 Total Study Area (Main Stream No. 1) = 230.24(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 25.943(CFS)
 Half street flow at end of street = 25.943(CFS)
 Depth of flow = 0.494(Ft.), Average velocity = 7.477(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Flow width (from curb towards crown)= 16.500(Ft.)

++++++
 Process from Point/Station 707.000 to Point/Station 708.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 987.000(Ft.)
Downstream point/station elevation = 967.000(Ft.)
Pipe length = 200.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 25.943(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 25.943(CFS)
Normal flow depth in pipe = 11.98(In.)
Flow top width inside pipe = 16.99(In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.80(Ft/s)
Travel time through pipe = 0.16 min.
Time of concentration (TC) = 9.39 min.

+++++
Process from Point/Station 707.000 to Point/Station 708.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 9.39 min.
Rainfall intensity = 2.586(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.862
Subarea runoff = 1.332(CFS) for 0.770(Ac.)
Total runoff = 27.274(CFS)
Effective area this stream = 12.23(Ac.)
Total Study Area (Main Stream No. 1) = 231.01(Ac.)
Area averaged Fm value = 0.109(In/Hr)

+++++
Process from Point/Station 708.000 to Point/Station 704.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 967.000(Ft.)
Downstream point/station elevation = 953.000(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 27.274(CFS)
Nearest computed pipe diameter = 18.00(In.)
Calculated individual pipe flow = 27.274(CFS)
Normal flow depth in pipe = 12.75(In.)
Flow top width inside pipe = 16.36(In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.39(Ft/s)
Travel time through pipe = 0.12 min.
Time of concentration (TC) = 9.51 min.

+++++
Process from Point/Station 708.000 to Point/Station 704.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 12.230(Ac.)
Runoff from this stream = 27.274(CFS)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Time of concentration = 9.51 min.
 Rainfall intensity = 2.566(In/Hr)
 Area averaged loss rate (Fm) = 0.1086(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2307
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
1	106.54	58.390	11.54	0.258	2.285
2	27.27	12.230	9.51	0.109	2.566
Qmax(1) =					
	1.000 *	1.000 *	106.540)	+	
	0.886 *	1.000 *	27.274)	+	130.694
Qmax(2) =					
	1.139 *	0.824 *	106.540)	+	
	1.000 *	1.000 *	27.274)	+	127.258

Total of 2 streams to confluence:
 Flow rates before confluence point:
 106.540 27.274
 Maximum flow rates at confluence using above data:
 130.694 127.258
 Area of streams before confluence:
 58.390 12.230
 Effective area values after confluence:
 70.620 60.352

Results of confluence:
 Total flow rate = 130.694(CFS)
 Time of concentration = 11.542 min.
 Effective stream area after confluence = 70.620(Ac.)
 Study area average Pervious fraction(Ap) = 0.841
 Study area average soil loss rate(Fm) = 0.232(In/Hr)
 Study area total (this main stream) = 70.62(Ac.)

 Process from Point/Station 704.000 to Point/Station 709.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 953.000(Ft.)
 Downstream point elevation = 876.000(Ft.)
 Channel length thru subarea = 1370.000(Ft.)
 Channel base width = 5.000(Ft.)
 Slope or 'Z' of left channel bank = 2.000
 Slope or 'Z' of right channel bank = 2.000
 Estimated mean flow rate at midpoint of channel = 142.477(CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 5.000(Ft.)
 Flow(q) thru subarea = 142.477(CFS)
 Depth of flow = 1.032(Ft.), Average velocity = 19.533(Ft/s)
 Channel flow top width = 9.130(Ft.)
 Flow Velocity = 19.53(Ft/s)
 Travel time = 1.17 min.
 Time of concentration = 12.71 min.
 Critical depth = 2.188(Ft.)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 2.157(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.800
Subarea runoff = 23.472(CFS) for 18.700(Ac.)
Total runoff = 154.167(CFS)
Effective area this stream = 89.32(Ac.)
Total Study Area (Main Stream No. 1) = 249.71(Ac.)
Area averaged Fm value = 0.239(In/Hr)
Depth of flow = 1.078(Ft.), Average velocity = 19.991(Ft/s)
Critical depth = 2.281(Ft.)

+++++
Process from Point/Station 704.000 to Point/Station 709.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 12.71 min.
Rainfall intensity = 2.157(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.799
Subarea runoff = 14.982(CFS) for 8.800(Ac.)
Total runoff = 169.148(CFS)
Effective area this stream = 98.12(Ac.)
Total Study Area (Main Stream No. 1) = 258.51(Ac.)
Area averaged Fm value = 0.241(In/Hr)

+++++
Process from Point/Station 704.000 to Point/Station 709.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 12.71 min.
Rainfall intensity = 2.157(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.801
Subarea runoff = 3.784(CFS) for 2.000(Ac.)
Total runoff = 172.932(CFS)
Effective area this stream = 100.12(Ac.)
Total Study Area (Main Stream No. 1) = 260.51(Ac.)
Area averaged Fm value = 0.238(In/Hr)

+++++
Process from Point/Station 800.000 to Point/Station 801.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 575.000 (Ft.)
 Top (of initial area) elevation = 1078.000 (Ft.)
 Bottom (of initial area) elevation = 986.000 (Ft.)
 Difference in elevation = 92.000 (Ft.)
 Slope = 0.16000 s(%)= 16.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.621 min.
 Rainfall intensity = 2.549 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.806
 Subarea runoff = 10.833 (CFS)
 Total initial stream area = 5.270 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265 (In/Hr)

++++++
 Process from Point/Station 900.000 to Point/Station 901.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 573.000 (Ft.)
 Top (of initial area) elevation = 1095.000 (Ft.)
 Bottom (of initial area) elevation = 946.000 (Ft.)
 Difference in elevation = 149.000 (Ft.)
 Slope = 0.26003 s(%)= 26.00
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 8.718 min.
 Rainfall intensity = 2.704 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.812
 Subarea runoff = 9.001 (CFS)
 Total initial stream area = 4.100 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265 (In/Hr)

++++++
 Process from Point/Station 900.000 to Point/Station 901.000
 **** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
 Time of concentration = 8.72 min.
 Rainfall intensity = 2.704 (In/Hr) for a 10.0 year storm
 Effective runoff coefficient used for area, (total area with modified

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

rational method) (Q=KCIA) is C = 0.812
Subarea runoff = 12.843(CFS) for 5.850(Ac.)
Total runoff = 21.843(CFS)
Effective area this stream = 9.95(Ac.)
Total Study Area (Main Stream No. 1) = 275.73(Ac.)
Area averaged Fm value = 0.265(In/Hr)

+++++
Process from Point/Station 902.000 to Point/Station 903.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 940.000(Ft.)
Downstream point/station elevation = 936.000(Ft.)
Pipe length = 335.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 21.843(CFS)
Nearest computed pipe diameter = 24.00(In.)
Calculated individual pipe flow = 21.843(CFS)
Normal flow depth in pipe = 17.53(In.)
Flow top width inside pipe = 21.30(In.)
Critical Depth = 20.04(In.)
Pipe flow velocity = 8.88(Ft/s)
Travel time through pipe = 0.63 min.
Time of concentration (TC) = 9.35 min.

+++++
Process from Point/Station 902.000 to Point/Station 903.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 9.35 min.
Rainfall intensity = 2.594(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.849
Subarea runoff = 27.366(CFS) for 12.410(Ac.)
Total runoff = 49.210(CFS)
Effective area this stream = 22.36(Ac.)
Total Study Area (Main Stream No. 1) = 288.14(Ac.)
Area averaged Fm value = 0.148(In/Hr)
End of computations, Total Study Area = 288.14 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.652
Area averaged SCS curve number = 77.8

ATTACHMENT A
Rational Method Hydrology
Existing Condition
(100-Year storm)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2005 Version 7.1
Rational Hydrology Study Date: 02/23/16

Roquet Ranch Project - TTM 19883
Proposed Condition
100-year storm

Program License Serial Number 4029

***** Hydrology Study Control Information *****

Rational hydrology study storm event year is 100.0
Computed rainfall intensity:
Storm year = 100.00 1 hour rainfall = 1.200 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

+++++
Process from Point/Station 100.000 to Point/Station 101.000
**** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274 (In/Hr)
Initial subarea data:
Initial area flow distance = 998.000 (Ft.)
Top (of initial area) elevation = 1015.600 (Ft.)
Bottom (of initial area) elevation = 951.000 (Ft.)
Difference in elevation = 64.600 (Ft.)
Slope = 0.06473 s(%)= 6.47
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.651 min.
Rainfall intensity = 3.386 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.827
Subarea runoff = 15.963 (CFS)
Total initial stream area = 5.700 (Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.274 (In/Hr)

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 943.000 (Ft.)
Downstream point/station elevation = 931.000 (Ft.)
Pipe length = 900.00 (Ft.) Manning's N = 0.013

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

No. of pipes = 1 Required pipe flow = 15.963(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 15.963(CFS)
Normal flow depth in pipe = 15.19(In.)
Flow top width inside pipe = 18.79(In.)
Critical Depth = 17.69(In.)
Pipe flow velocity = 8.57(Ft/s)
Travel time through pipe = 1.75 min.
Time of concentration (TC) = 12.40 min.

+++++
Process from Point/Station 101.000 to Point/Station 102.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 12.40 min.
Rainfall intensity = 3.090(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.829
Subarea runoff = 15.178(CFS) for 6.460(Ac.)
Total runoff = 31.141(CFS)
Effective area this stream = 12.16(Ac.)
Total Study Area (Main Stream No. 1) = 12.16(Ac.)
Area averaged Fm value = 0.245(In/Hr)

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 931.000(Ft.)
Downstream point/station elevation = 915.000(Ft.)
Pipe length = 1010.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 31.141(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 31.141(CFS)
Normal flow depth in pipe = 18.26(In.)
Flow top width inside pipe = 25.27(In.)
Critical Depth = 23.10(In.)
Pipe flow velocity = 10.89(Ft/s)
Travel time through pipe = 1.55 min.
Time of concentration (TC) = 13.95 min.

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 13.95 min.

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Rainfall intensity = 2.880(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.826
Subarea runoff = 10.630(CFS) for 5.400(Ac.)
Total runoff = 41.771(CFS)
Effective area this stream = 17.56(Ac.)
Total Study Area (Main Stream No. 1) = 17.56(Ac.)
Area averaged Fm value = 0.237(In/Hr)

+++++
Process from Point/Station 102.000 to Point/Station 103.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 13.95 min.
Rainfall intensity = 2.880(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.827
Subarea runoff = 10.250(CFS) for 4.280(Ac.)
Total runoff = 52.021(CFS)
Effective area this stream = 21.84(Ac.)
Total Study Area (Main Stream No. 1) = 21.84(Ac.)
Area averaged Fm value = 0.233(In/Hr)

+++++
Process from Point/Station 103.000 to Point/Station 104.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 915.000(Ft.)
Downstream point/station elevation = 910.000(Ft.)
Pipe length = 440.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 52.021(CFS)
Nearest computed pipe diameter = 33.00(In.)
Calculated individual pipe flow = 52.021(CFS)
Normal flow depth in pipe = 24.98(In.)
Flow top width inside pipe = 28.30(In.)
Critical Depth = 28.39(In.)
Pipe flow velocity = 10.77(Ft/s)
Travel time through pipe = 0.68 min.
Time of concentration (TC) = 14.63 min.

+++++
Process from Point/Station 103.000 to Point/Station 104.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 14.63 min.
Rainfall intensity = 2.799(In/Hr) for a 100.0 year storm

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.826
Subarea runoff = 7.319(CFS) for 3.840(Ac.)
Total runoff = 59.341(CFS)
Effective area this stream = 25.68(Ac.)
Total Study Area (Main Stream No. 1) = 25.68(Ac.)
Area averaged Fm value = 0.231(In/Hr)

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 910.000(Ft.)
Downstream point/station elevation = 905.000(Ft.)
Pipe length = 100.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 59.341(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 59.341(CFS)
Normal flow depth in pipe = 19.24(In.)
Flow top width inside pipe = 24.44(In.)
Critical depth could not be calculated.
Pipe flow velocity = 19.58(Ft/s)
Travel time through pipe = 0.09 min.
Time of concentration (TC) = 14.71 min.

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** SUBAREA FLOW ADDITION ****

PARK subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.8500 Max loss rate(Fm)= 0.466(In/Hr)
Time of concentration = 14.71 min.
Rainfall intensity = 2.789(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.822
Subarea runoff = 2.033(CFS) for 1.080(Ac.)
Total runoff = 61.374(CFS)
Effective area this stream = 26.76(Ac.)
Total Study Area (Main Stream No. 1) = 26.76(Ac.)
Area averaged Fm value = 0.241(In/Hr)

++++
Process from Point/Station 104.000 to Point/Station 105.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 26.760(Ac.)
Runoff from this stream = 61.374(CFS)
Time of concentration = 14.71 min.
Rainfall intensity = 2.789(In/Hr)
Area averaged loss rate (Fm) = 0.2408(In/Hr)
Area averaged Pervious ratio (Ap) = 0.4395

++++

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Process from Point/Station 106.000 to Point/Station 107.000
**** INITIAL AREA EVALUATION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274 (In/Hr)
Initial subarea data:
Initial area flow distance = 855.000 (Ft.)
Top (of initial area) elevation = 998.000 (Ft.)
Bottom (of initial area) elevation = 962.000 (Ft.)
Difference in elevation = 36.000 (Ft.)
Slope = 0.04211 s(%)= 4.21
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.911 min.
Rainfall intensity = 3.337 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.826
Subarea runoff = 12.322 (CFS)
Total initial stream area = 4.470 (Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.274 (In/Hr)

+++++
Process from Point/Station 107.000 to Point/Station 105.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 955.000 (Ft.)
Downstream point/station elevation = 905.000 (Ft.)
Pipe length = 950.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 12.322 (CFS)
Nearest computed pipe diameter = 15.00 (In.)
Calculated individual pipe flow = 12.322 (CFS)
Normal flow depth in pipe = 10.44 (In.)
Flow top width inside pipe = 13.80 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 13.51 (Ft/s)
Travel time through pipe = 1.17 min.
Time of concentration (TC) = 12.08 min.

+++++
Process from Point/Station 107.000 to Point/Station 105.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274 (In/Hr)
Time of concentration = 12.08 min.
Rainfall intensity = 3.139 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.821
Subarea runoff = 10.238 (CFS) for 4.280 (Ac.)
Total runoff = 22.560 (CFS)
Effective area this stream = 8.75 (Ac.)
Total Study Area (Main Stream No. 1) = 35.51 (Ac.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Area averaged Fm value = 0.274 (In/Hr)

+++++
Process from Point/Station 107.000 to Point/Station 105.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
Stream flow area = 8.750 (Ac.)
Runoff from this stream = 22.560 (CFS)
Time of concentration = 12.08 min.
Rainfall intensity = 3.139 (In/Hr)
Area averaged loss rate (Fm) = 0.2740 (In/Hr)
Area averaged Pervious ratio (Ap) = 0.5000

+++++
Process from Point/Station 108.000 to Point/Station 109.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 69.00
Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.055 (In/Hr)
Initial subarea data:
Initial area flow distance = 525.000 (Ft.)
Top (of initial area) elevation = 994.400 (Ft.)
Bottom (of initial area) elevation = 932.000 (Ft.)
Difference in elevation = 62.400 (Ft.)
Slope = 0.11886 s(%) = 11.89
TC = $k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$
Initial area time of concentration = 5.701 min.
Rainfall intensity = 4.926 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.890
Subarea runoff = 5.042 (CFS)
Total initial stream area = 1.150 (Ac.)
Pervious area fraction = 0.100
Initial area Fm value = 0.055 (In/Hr)

+++++
Process from Point/Station 109.000 to Point/Station 110.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 932.000 (Ft.)
End of street segment elevation = 916.800 (Ft.)
Length of street segment = 610.000 (Ft.)
Height of curb above gutter flowline = 6.0 (In.)
Width of half street (curb to crown) = 16.500 (Ft.)
Distance from crown to crossfall grade break = 2.000 (Ft.)
Slope from gutter to grade break (v/hz) = 0.020
Slope from grade break to crown (v/hz) = 0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line = 13.500 (Ft.)
Slope from curb to property line (v/hz) = 0.025
Gutter width = 2.000 (Ft.)
Gutter hike from flowline = 2.000 (In.)
Manning's N in gutter = 0.0150
Manning's N from gutter to grade break = 0.0150
Manning's N from grade break to crown = 0.0150

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Estimated mean flow rate at midpoint of street = 7.681(CFS)
 Depth of flow = 0.389(Ft.), Average velocity = 4.151(Ft/s)
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 13.128(Ft.)
 Flow velocity = 4.15(Ft/s)
 Travel time = 2.45 min. TC = 8.15 min.
 Adding area flow to street
 COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Rainfall intensity = 3.975(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.888
 Subarea runoff = 5.191(CFS) for 1.750(Ac.)
 Total runoff = 10.233(CFS)
 Effective area this stream = 2.90(Ac.)
 Total Study Area (Main Stream No. 1) = 38.41(Ac.)
 Area averaged Fm value = 0.055(In/Hr)
 Street flow at end of street = 10.233(CFS)
 Half street flow at end of street = 10.233(CFS)
 Depth of flow = 0.422(Ft.), Average velocity = 4.447(Ft/s)
 Flow width (from curb towards crown)= 14.747(Ft.)

++++++
 Process from Point/Station 110.000 to Point/Station 105.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 909.000(Ft.)
 Downstream point/station elevation = 905.000(Ft.)
 Pipe length = 100.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 10.233(CFS)
 Nearest computed pipe diameter = 15.00(In.)
 Calculated individual pipe flow = 10.233(CFS)
 Normal flow depth in pipe = 10.08(In.)
 Flow top width inside pipe = 14.09(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 11.68(Ft/s)
 Travel time through pipe = 0.14 min.
 Time of concentration (TC) = 8.29 min.

++++++
 Process from Point/Station 110.000 to Point/Station 105.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 3
 Stream flow area = 2.900(Ac.)
 Runoff from this stream = 10.233(CFS)
 Time of concentration = 8.29 min.
 Rainfall intensity = 3.934(In/Hr)
 Area averaged loss rate (Fm) = 0.0548(In/Hr)
 Area averaged Pervious ratio (Ap) = 0.1000
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
------------	-----------------	------------	----------	------------	----------------------------

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

1	61.37	26.760	14.71	0.241	2.789
2	22.56	8.750	12.08	0.274	3.139
3	10.23	2.900	8.29	0.055	3.934
Qmax(1) =					
	1.000 *	1.000 *	61.374)	+	
	0.878 *	1.000 *	22.560)	+	
	0.705 *	1.000 *	10.233)	+	88.393
Qmax(2) =					
	1.137 *	0.821 *	61.374)	+	
	1.000 *	1.000 *	22.560)	+	
	0.795 *	1.000 *	10.233)	+	88.019
Qmax(3) =					
	1.449 *	0.564 *	61.374)	+	
	1.278 *	0.686 *	22.560)	+	
	1.000 *	1.000 *	10.233)	+	80.153

Total of 3 streams to confluence:
Flow rates before confluence point:
61.374 22.560 10.233
Maximum flow rates at confluence using above data:
88.393 88.019 80.153
Area of streams before confluence:
26.760 8.750 2.900
Effective area values after confluence:
38.410 33.629 23.988
Results of confluence:
Total flow rate = 88.393(CFS)
Time of concentration = 14.712 min.
Effective stream area after confluence = 38.410(Ac.)
Study area average Pervious fraction(Ap) = 0.428
Study area average soil loss rate(Fm) = 0.234(In/Hr)
Study area total (this main stream) = 38.41(Ac.)

+++++
Process from Point/Station 105.000 to Point/Station 111.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 905.000(Ft.)
Downstream point/station elevation = 904.000(Ft.)
Pipe length = 60.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 88.393(CFS)
Nearest computed pipe diameter = 39.00(In.)
Calculated individual pipe flow = 88.393(CFS)
Normal flow depth in pipe = 27.09(In.)
Flow top width inside pipe = 35.92(In.)
Critical Depth = 34.95(In.)
Pipe flow velocity = 14.36(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 14.78 min.

+++++
Process from Point/Station 105.000 to Point/Station 111.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
Stream flow area = 38.410(Ac.)
Runoff from this stream = 88.393(CFS)
Time of concentration = 14.78 min.
Rainfall intensity = 2.781(In/Hr)
Area averaged loss rate (Fm) = 0.2343(In/Hr)
Area averaged Pervious ratio (Ap) = 0.4276

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

+++++
 Process from Point/Station 112.000 to Point/Station 113.000
 **** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 990.000 (Ft.)
 Top (of initial area) elevation = 1100.000 (Ft.)
 Bottom (of initial area) elevation = 925.000 (Ft.)
 Difference in elevation = 175.000 (Ft.)
 Slope = 0.17677 s(%)= 17.68
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 11.720 min.
 Rainfall intensity = 3.197 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.825
 Subarea runoff = 20.053 (CFS)
 Total initial stream area = 7.600 (Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265 (In/Hr)

+++++
 Process from Point/Station 113.000 to Point/Station 111.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 918.000 (Ft.)
 Downstream point/station elevation = 904.000 (Ft.)
 Pipe length = 150.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 20.053 (CFS)
 Nearest computed pipe diameter = 18.00 (In.)
 Calculated individual pipe flow = 20.053 (CFS)
 Normal flow depth in pipe = 10.31 (In.)
 Flow top width inside pipe = 17.81 (In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 19.16 (Ft/s)
 Travel time through pipe = 0.13 min.
 Time of concentration (TC) = 11.85 min.

+++++
 Process from Point/Station 113.000 to Point/Station 111.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 7.600 (Ac.)
 Runoff from this stream = 20.053 (CFS)
 Time of concentration = 11.85 min.
 Rainfall intensity = 3.176 (In/Hr)
 Area averaged loss rate (Fm) = 0.2651 (In/Hr)
 Area averaged Pervious ratio (Ap) = 1.0000
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
------------	-----------------	------------	----------	------------	----------------------------

**Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B**

1	88.39	38.410	14.78	0.234	2.781
2	20.05	7.600	11.85	0.265	3.176
Qmax(1) =					
	1.000 *	1.000 *	88.393)	+	
	0.864 *	1.000 *	20.053)	+	105.729
Qmax(2) =					
	1.155 *	0.802 *	88.393)	+	
	1.000 *	1.000 *	20.053)	+	101.891

Total of 2 streams to confluence:
 Flow rates before confluence point:
 88.393 20.053
 Maximum flow rates at confluence using above data:
 105.729 101.891
 Area of streams before confluence:
 38.410 7.600
 Effective area values after confluence:
 46.010 38.393

Results of confluence:
 Total flow rate = 105.729(CFS)
 Time of concentration = 14.782 min.
 Effective stream area after confluence = 46.010 (Ac.)
 Study area average Pervious fraction (Ap) = 0.522
 Study area average soil loss rate (Fm) = 0.239 (In/Hr)
 Study area total (this main stream) = 46.01 (Ac.)

 Process from Point/Station 111.000 to Point/Station 120.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 904.000 (Ft.)
 Downstream point/station elevation = 899.000 (Ft.)
 Pipe length = 715.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 105.729 (CFS)
 Nearest computed pipe diameter = 48.00 (In.)
 Calculated individual pipe flow = 105.729 (CFS)
 Normal flow depth in pipe = 34.97 (In.)
 Flow top width inside pipe = 42.69 (In.)
 Critical Depth = 37.35 (In.)
 Pipe flow velocity = 10.79 (Ft/s)
 Travel time through pipe = 1.10 min.
 Time of concentration (TC) = 15.89 min.

 Process from Point/Station 111.000 to Point/Station 120.000
 **** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1
 Stream flow area = 46.010 (Ac.)
 Runoff from this stream = 105.729 (CFS)
 Time of concentration = 15.89 min.
 Rainfall intensity = 2.664 (In/Hr)
 Area averaged loss rate (Fm) = 0.2394 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5222

 Process from Point/Station 121.000 to Point/Station 122.000
 **** INITIAL AREA EVALUATION ****

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274 (In/Hr)
Initial subarea data:
Initial area flow distance = 795.000(Ft.)
Top (of initial area) elevation = 1075.000(Ft.)
Bottom (of initial area) elevation = 1058.000(Ft.)
Difference in elevation = 17.000(Ft.)
Slope = 0.02138 s(%)= 2.14
TC = k(0.389)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 12.136 min.
Rainfall intensity = 3.131(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.821
Subarea runoff = 11.466(CFS)
Total initial stream area = 4.460 (Ac.)
Pervious area fraction = 0.500
Initial area Fm value = 0.274(In/Hr)

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219 (In/Hr)
Time of concentration = 12.14 min.
Rainfall intensity = 3.131(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.831
Subarea runoff = 18.237(CFS) for 6.960 (Ac.)
Total runoff = 29.704(CFS)
Effective area this stream = 11.42 (Ac.)
Total Study Area (Main Stream No. 1) = 57.43 (Ac.)
Area averaged Fm value = 0.241 (In/Hr)

+++++
Process from Point/Station 121.000 to Point/Station 122.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055 (In/Hr)
Time of concentration = 12.14 min.
Rainfall intensity = 3.131(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.837
Subarea runoff = 4.401(CFS) for 1.590 (Ac.)
Total runoff = 34.105(CFS)
Effective area this stream = 13.01 (Ac.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Total Study Area (Main Stream No. 1) = 59.02 (Ac.)
Area averaged Fm value = 0.218 (In/Hr)

+++++
Process from Point/Station 122.000 to Point/Station 123.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 1050.000 (Ft.)
Downstream point/station elevation = 980.000 (Ft.)
Pipe length = 1850.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 34.105 (CFS)
Nearest computed pipe diameter = 24.00 (In.)
Calculated individual pipe flow = 34.105 (CFS)
Normal flow depth in pipe = 15.87 (In.)
Flow top width inside pipe = 22.72 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 15.47 (Ft/s)
Travel time through pipe = 1.99 min.
Time of concentration (TC) = 14.13 min.

+++++
Process from Point/Station 122.000 to Point/Station 123.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(5 - 7 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.5000 Max loss rate(Fm)= 0.274 (In/Hr)
Time of concentration = 14.13 min.
Rainfall intensity = 2.858 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.825
Subarea runoff = 13.615 (CFS) for 7.230 (Ac.)
Total runoff = 47.720 (CFS)
Effective area this stream = 20.24 (Ac.)
Total Study Area (Main Stream No. 1) = 66.25 (Ac.)
Area averaged Fm value = 0.238 (In/Hr)

+++++
Process from Point/Station 123.000 to Point/Station 124.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 980.000 (Ft.)
Downstream point/station elevation = 932.000 (Ft.)
Pipe length = 785.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 47.720 (CFS)
Nearest computed pipe diameter = 24.00 (In.)
Calculated individual pipe flow = 47.720 (CFS)
Normal flow depth in pipe = 17.04 (In.)
Flow top width inside pipe = 21.78 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.00 (Ft/s)
Travel time through pipe = 0.65 min.
Time of concentration (TC) = 14.78 min.

+++++

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Process from Point/Station 123.000 to Point/Station 124.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(8 - 10 dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.4000 Max loss rate(Fm)= 0.219(In/Hr)
Time of concentration = 14.78 min.
Rainfall intensity = 2.781(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.824
Subarea runoff = 4.692(CFS) for 2.640(Ac.)
Total runoff = 52.413(CFS)
Effective area this stream = 22.88(Ac.)
Total Study Area (Main Stream No. 1) = 68.89(Ac.)
Area averaged Fm value = 0.236(In/Hr)

+++++
Process from Point/Station 123.000 to Point/Station 124.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 14.78 min.
Rainfall intensity = 2.781(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.822
Subarea runoff = 8.084(CFS) for 3.570(Ac.)
Total runoff = 60.496(CFS)
Effective area this stream = 26.45(Ac.)
Total Study Area (Main Stream No. 1) = 72.46(Ac.)
Area averaged Fm value = 0.240(In/Hr)

+++++
Process from Point/Station 124.000 to Point/Station 120.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 932.000(Ft.)
Downstream point/station elevation = 898.000(Ft.)
Pipe length = 1070.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 60.496(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 60.496(CFS)
Normal flow depth in pipe = 20.81(In.)
Flow top width inside pipe = 27.66(In.)
Critical depth could not be calculated.
Pipe flow velocity = 16.65(Ft/s)
Travel time through pipe = 1.07 min.
Time of concentration (TC) = 15.85 min.

+++++
Process from Point/Station 124.000 to Point/Station 120.000

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 26.450 (Ac.)
 Runoff from this stream = 60.496 (CFS)
 Time of concentration = 15.85 min.
 Rainfall intensity = 2.667 (In/Hr)
 Area averaged loss rate (Fm) = 0.2397 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.5071
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
1	105.73	46.010	15.89	0.239	2.664
2	60.50	26.450	15.85	0.240	2.667
Qmax(1) =					
	1.000 *	1.000 *	105.729)	+	
	0.999 *	1.000 *	60.496)	+	166.146
Qmax(2) =					
	1.001 *	0.998 *	105.729)	+	
	1.000 *	1.000 *	60.496)	+	166.153

Total of 2 streams to confluence:
 Flow rates before confluence point:
 105.729 60.496
 Maximum flow rates at confluence using above data:
 166.146 166.153
 Area of streams before confluence:
 46.010 26.450
 Effective area values after confluence:
 72.460 72.368
 Results of confluence:
 Total flow rate = 166.153 (CFS)
 Time of concentration = 15.855 min.
 Effective stream area after confluence = 72.368 (Ac.)
 Study area average Pervious fraction (Ap) = 0.517
 Study area average soil loss rate (Fm) = 0.239 (In/Hr)
 Study area total (this main stream) = 72.46 (Ac.)

 Process from Point/Station 200.000 to Point/Station 201.000
 **** INITIAL AREA EVALUATION ****

RESIDENTIAL (11+ dwl/acre)
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 69.00
 Pervious ratio (Ap) = 0.2000 Max loss rate (Fm) = 0.110 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 825.000 (Ft.)
 Top (of initial area) elevation = 914.700 (Ft.)
 Bottom (of initial area) elevation = 910.300 (Ft.)
 Difference in elevation = 4.400 (Ft.)
 Slope = 0.00533 s (%) = 0.53
 $TC = k(0.324) * [(length^3) / (elevation\ change)]^{0.2}$
 Initial area time of concentration = 13.543 min.
 Rainfall intensity = 2.931 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.866

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Subarea runoff = 12.392 (CFS)
Total initial stream area = 4.880 (Ac.)
Pervious area fraction = 0.200
Initial area Fm value = 0.110 (In/Hr)

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 903.000 (Ft.)
Downstream point/station elevation = 899.000 (Ft.)
Pipe length = 506.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 12.392 (CFS)
Nearest computed pipe diameter = 21.00 (In.)
Calculated individual pipe flow = 12.392 (CFS)
Normal flow depth in pipe = 15.28 (In.)
Flow top width inside pipe = 18.70 (In.)
Critical Depth = 15.73 (In.)
Pipe flow velocity = 6.61 (Ft/s)
Travel time through pipe = 1.28 min.
Time of concentration (TC) = 14.82 min.

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(11+ dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110 (In/Hr)
Time of concentration = 14.82 min.
Rainfall intensity = 2.777 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.864
Subarea runoff = 13.775 (CFS) for 6.020 (Ac.)
Total runoff = 26.167 (CFS)
Effective area this stream = 10.90 (Ac.)
Total Study Area (Main Stream No. 1) = 83.36 (Ac.)
Area averaged Fm value = 0.110 (In/Hr)

+++++
Process from Point/Station 201.000 to Point/Station 202.000
**** SUBAREA FLOW ADDITION ****

RESIDENTIAL(11+ dwl/acre)
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110 (In/Hr)
Time of concentration = 14.82 min.
Rainfall intensity = 2.777 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.864
Subarea runoff = 24.487 (CFS) for 10.200 (Ac.)
Total runoff = 50.654 (CFS)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Effective area this stream = 21.10 (Ac.)
 Total Study Area (Main Stream No. 1) = 93.56 (Ac.)
 Area averaged Fm value = 0.110 (In/Hr)

+++++
 Process from Point/Station 202.000 to Point/Station 203.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 899.000 (Ft.)
 Downstream point/station elevation = 857.000 (Ft.)
 Pipe length = 675.00 (Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 50.654 (CFS)
 Nearest computed pipe diameter = 24.00 (In.)
 Calculated individual pipe flow = 50.654 (CFS)
 Normal flow depth in pipe = 17.77 (In.)
 Flow top width inside pipe = 21.05 (In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 20.32 (Ft/s)
 Travel time through pipe = 0.55 min.
 Time of concentration (TC) = 15.37 min.

+++++
 Process from Point/Station 202.000 to Point/Station 203.000
 **** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 86.00
 Pervious ratio (Ap) = 1.0000 Max loss rate (Fm) = 0.265 (In/Hr)
 Time of concentration = 15.37 min.
 Rainfall intensity = 2.717 (In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.859
 Subarea runoff = 4.037 (CFS) for 2.350 (Ac.)
 Total runoff = 54.691 (CFS)
 Effective area this stream = 23.45 (Ac.)
 Total Study Area (Main Stream No. 1) = 95.91 (Ac.)
 Area averaged Fm value = 0.125 (In/Hr)

+++++
 Process from Point/Station 300.000 to Point/Station 301.000
 **** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil (AMC 2) = 69.00
 Pervious ratio (Ap) = 0.1000 Max loss rate (Fm) = 0.055 (In/Hr)
 Initial subarea data:
 Initial area flow distance = 1000.000 (Ft.)
 Top (of initial area) elevation = 920.000 (Ft.)
 Bottom (of initial area) elevation = 857.000 (Ft.)
 Difference in elevation = 63.000 (Ft.)
 Slope = 0.06300 s(%) = 6.30
 $TC = k(0.304) * [(length^3) / (elevation\ change)]^{0.2}$

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Initial area time of concentration = 8.375 min.
 Rainfall intensity = 3.911(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.887
 Subarea runoff = 10.862(CFS)
 Total initial stream area = 3.130(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.055(In/Hr)

 Process from Point/Station 301.000 to Point/Station 302.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 851.000(Ft.)
 Downstream point/station elevation = 846.000(Ft.)
 Pipe length = 1250.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 10.862(CFS)
 Nearest computed pipe diameter = 24.00(In.)
 Calculated individual pipe flow = 10.862(CFS)
 Normal flow depth in pipe = 15.63(In.)
 Flow top width inside pipe = 22.87(In.)
 Critical Depth = 14.18(In.)
 Pipe flow velocity = 5.01(Ft/s)
 Travel time through pipe = 4.16 min.
 Time of concentration (TC) = 12.53 min.

 Process from Point/Station 301.000 to Point/Station 302.000
 **** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
 Time of concentration = 12.53 min.
 Rainfall intensity = 3.071(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.884
 Subarea runoff = 7.811(CFS) for 3.750(Ac.)
 Total runoff = 18.673(CFS)
 Effective area this stream = 6.88(Ac.)
 Total Study Area (Main Stream No. 1) = 102.79(Ac.)
 Area averaged Fm value = 0.055(In/Hr)

 Process from Point/Station 302.000 to Point/Station 303.000
 **** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 846.000(Ft.)
 Downstream point/station elevation = 842.000(Ft.)
 Pipe length = 60.00(Ft.) Manning's N = 0.013
 No. of pipes = 1 Required pipe flow = 18.673(CFS)
 Nearest computed pipe diameter = 18.00(In.)
 Calculated individual pipe flow = 18.673(CFS)
 Normal flow depth in pipe = 10.97(In.)
 Flow top width inside pipe = 17.56(In.)
 Critical depth could not be calculated.
 Pipe flow velocity = 16.54(Ft/s)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Travel time through pipe = 0.06 min.
Time of concentration (TC) = 12.59 min.

+++++
Process from Point/Station 302.000 to Point/Station 303.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 12.59 min.
Rainfall intensity = 3.062(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.880
Subarea runoff = 1.103(CFS) for 0.460(Ac.)
Total runoff = 19.776(CFS)
Effective area this stream = 7.34(Ac.)
Total Study Area (Main Stream No. 1) = 103.25(Ac.)
Area averaged Fm value = 0.068(In/Hr)

+++++
Process from Point/Station 400.000 to Point/Station 401.000
**** INITIAL AREA EVALUATION ****

APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
Initial subarea data:
Initial area flow distance = 615.000(Ft.)
Top (of initial area) elevation = 862.000(Ft.)
Bottom (of initial area) elevation = 852.000(Ft.)
Difference in elevation = 10.000(Ft.)
Slope = 0.01626 s(%)= 1.63
TC = k(0.324)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.635 min.
Rainfall intensity = 3.595(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.873
Subarea runoff = 7.027(CFS)
Total initial stream area = 2.240(Ac.)
Pervious area fraction = 0.200
Initial area Fm value = 0.110(In/Hr)

+++++
Process from Point/Station 500.000 to Point/Station 501.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Initial subarea data:
 Initial area flow distance = 847.000(Ft.)
 Top (of initial area) elevation = 1393.600(Ft.)
 Bottom (of initial area) elevation = 1044.000(Ft.)
 Difference in elevation = 349.600(Ft.)
 Slope = 0.41275 s(%)= 41.28
 $TC = k(0.525)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 9.293 min.
 Rainfall intensity = 3.674(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.835
 Subarea runoff = 16.108(CFS)
 Total initial stream area = 5.250(Ac.)
 Pervious area fraction = 1.000
 Initial area Fm value = 0.265(In/Hr)

++++++
 Process from Point/Station 501.000 to Point/Station 502.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1044.000(Ft.)
 Downstream point elevation = 995.000(Ft.)
 Channel length thru subarea = 895.000(Ft.)
 Channel base width = 2.000(Ft.)
 Slope or 'Z' of left channel bank = 2.000
 Slope or 'Z' of right channel bank = 2.000
 Estimated mean flow rate at midpoint of channel = 32.442(CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 3.000(Ft.)
 Flow(q) thru subarea = 32.442(CFS)
 Depth of flow = 0.693(Ft.), Average velocity = 13.819(Ft/s)
 Channel flow top width = 4.773(Ft.)
 Flow Velocity = 13.82(Ft/s)
 Travel time = 1.08 min.
 Time of concentration = 10.37 min.
 Critical depth = 1.328(Ft.)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Rainfall intensity = 3.440(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified
 rational method) (Q=KCIA) is C = 0.831
 Subarea runoff = 32.608(CFS) for 11.800(Ac.)
 Total runoff = 48.716(CFS)
 Effective area this stream = 17.05(Ac.)
 Total Study Area (Main Stream No. 1) = 122.54(Ac.)
 Area averaged Fm value = 0.265(In/Hr)
 Depth of flow = 0.852(Ft.), Average velocity = 15.432(Ft/s)
 Critical depth = 1.625(Ft.)

++++++
 Process from Point/Station 502.000 to Point/Station 503.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 995.000(Ft.)
 Downstream point elevation = 984.000(Ft.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Channel length thru subarea = 505.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 0.000
Estimated mean flow rate at midpoint of channel = 52.977(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 52.977(CFS)
Depth of flow = 1.355(Ft.), Average velocity = 11.657(Ft/s)
Channel flow top width = 4.709(Ft.)
Flow Velocity = 11.66(Ft/s)
Travel time = 0.72 min.
Time of concentration = 11.09 min.
Critical depth = 2.016(Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 3.304(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.828
Subarea runoff = 8.440(CFS) for 3.850(Ac.)
Total runoff = 57.156(CFS)
Effective area this stream = 20.90(Ac.)
Total Study Area (Main Stream No. 1) = 126.39(Ac.)
Area averaged Fm value = 0.265(In/Hr)
Depth of flow = 1.410(Ft.), Average velocity = 11.884(Ft/s)
Critical depth = 2.094(Ft.)

+++++
Process from Point/Station 503.000 to Point/Station 504.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 984.000(Ft.)
Downstream point elevation = 939.000(Ft.)
Channel length thru subarea = 688.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 63.906(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 63.906(CFS)
Depth of flow = 0.933(Ft.), Average velocity = 17.711(Ft/s)
Channel flow top width = 5.733(Ft.)
Flow Velocity = 17.71(Ft/s)
Travel time = 0.65 min.
Time of concentration = 11.74 min.
Critical depth = 1.859(Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 3.193(In/Hr) for a 100.0 year storm

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.825
 Subarea runoff = 13.416(CFS) for 5.880(Ac.)
 Total runoff = 70.572(CFS)
 Effective area this stream = 26.78(Ac.)
 Total Study Area (Main Stream No. 1) = 132.27(Ac.)
 Area averaged Fm value = 0.265(In/Hr)
 Depth of flow = 0.980(Ft.), Average velocity = 18.184(Ft/s)
 Critical depth = 1.953(Ft.)

+++++
 Process from Point/Station 504.000 to Point/Station 505.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 939.000(Ft.)
 Downstream point elevation = 905.000(Ft.)
 Channel length thru subarea = 1140.000(Ft.)
 Channel base width = 2.000(Ft.)
 Slope or 'Z' of left channel bank = 2.000
 Slope or 'Z' of right channel bank = 2.000
 Estimated mean flow rate at midpoint of channel = 72.857(CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 3.000(Ft.)
 Flow(q) thru subarea = 72.857(CFS)
 Depth of flow = 1.204(Ft.), Average velocity = 13.727(Ft/s)
 Channel flow top width = 6.816(Ft.)
 Flow Velocity = 13.73(Ft/s)
 Travel time = 1.38 min.
 Time of concentration = 13.13 min.
 Critical depth = 1.969(Ft.)
 Adding area flow to channel
 UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Rainfall intensity = 2.987(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area, (total area with modified rational method) (Q=KCIA) is C = 0.820
 Subarea runoff = 4.478(CFS) for 3.860(Ac.)
 Total runoff = 75.050(CFS)
 Effective area this stream = 30.64(Ac.)
 Total Study Area (Main Stream No. 1) = 136.13(Ac.)
 Area averaged Fm value = 0.265(In/Hr)
 Depth of flow = 1.221(Ft.), Average velocity = 13.834(Ft/s)
 Critical depth = 2.000(Ft.)

+++++
 Process from Point/Station 504.000 to Point/Station 505.000
 **** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 86.00
 Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
 Time of concentration = 13.13 min.

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Rainfall intensity = 2.987(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.820
Subarea runoff = 9.430(CFS) for 3.850 (Ac.)
Total runoff = 84.480(CFS)
Effective area this stream = 34.49 (Ac.)
Total Study Area (Main Stream No. 1) = 139.98 (Ac.)
Area averaged Fm value = 0.265 (In/Hr)

+++++
Process from Point/Station 600.000 to Point/Station 601.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055 (In/Hr)
Initial subarea data:
Initial area flow distance = 865.000 (Ft.)
Top (of initial area) elevation = 994.400 (Ft.)
Bottom (of initial area) elevation = 913.600 (Ft.)
Difference in elevation = 80.800 (Ft.)
Slope = 0.09341 s(%)= 9.34
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 7.305 min.
Rainfall intensity = 4.245 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.888
Subarea runoff = 16.519 (CFS)
Total initial stream area = 4.380 (Ac.)
Pervious area fraction = 0.100
Initial area Fm value = 0.055 (In/Hr)

+++++
Process from Point/Station 600.000 to Point/Station 601.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055 (In/Hr)
Time of concentration = 7.30 min.
Rainfall intensity = 4.245 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.888
Subarea runoff = 17.123 (CFS) for 4.540 (Ac.)
Total runoff = 33.642 (CFS)
Effective area this stream = 8.92 (Ac.)
Total Study Area (Main Stream No. 1) = 148.90 (Ac.)
Area averaged Fm value = 0.055 (In/Hr)

+++++
Process from Point/Station 601.000 to Point/Station 602.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Upstream point/station elevation = 908.000 (Ft.)
Downstream point/station elevation = 885.000 (Ft.)
Pipe length = 300.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 33.642 (CFS)
Nearest computed pipe diameter = 21.00 (In.)
Calculated individual pipe flow = 33.642 (CFS)
Normal flow depth in pipe = 13.78 (In.)
Flow top width inside pipe = 19.95 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 20.10 (Ft/s)
Travel time through pipe = 0.25 min.
Time of concentration (TC) = 7.55 min.

+++++
Process from Point/Station 601.000 to Point/Station 602.000
**** SUBAREA FLOW ADDITION ****

APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil (AMC 2) = 69.00
Pervious ratio (Ap) = 0.2000 Max loss rate (Fm) = 0.110 (In/Hr)
Time of concentration = 7.55 min.
Rainfall intensity = 4.161 (In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.882
Subarea runoff = 36.513 (CFS) for 10.200 (Ac.)
Total runoff = 70.155 (CFS)
Effective area this stream = 19.12 (Ac.)
Total Study Area (Main Stream No. 1) = 159.10 (Ac.)
Area averaged Fm value = 0.084 (In/Hr)

+++++
Process from Point/Station 602.000 to Point/Station 603.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 885.000 (Ft.)
Downstream point/station elevation = 882.000 (Ft.)
Pipe length = 80.00 (Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 70.155 (CFS)
Nearest computed pipe diameter = 30.00 (In.)
Calculated individual pipe flow = 70.155 (CFS)
Normal flow depth in pipe = 21.89 (In.)
Flow top width inside pipe = 26.65 (In.)
Critical depth could not be calculated.
Pipe flow velocity = 18.26 (Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 7.63 min.

+++++
Process from Point/Station 602.000 to Point/Station 603.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 7.63 min.
Rainfall intensity = 4.137(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.879
Subarea runoff = 4.083(CFS) for 1.290(Ac.)
Total runoff = 74.238(CFS)
Effective area this stream = 20.41(Ac.)
Total Study Area (Main Stream No. 1) = 160.39(Ac.)
Area averaged Fm value = 0.095(In/Hr)

++++
Process from Point/Station 700.000 to Point/Station 701.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Initial subarea data:
Initial area flow distance = 998.000(Ft.)
Top (of initial area) elevation = 1477.000(Ft.)
Bottom (of initial area) elevation = 1082.000(Ft.)
Difference in elevation = 395.000(Ft.)
Slope = 0.39579 s(%)= 39.58
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.007 min.
Rainfall intensity = 3.515(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.832
Subarea runoff = 15.032(CFS)
Total initial stream area = 5.140(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.265(In/Hr)

++++
Process from Point/Station 701.000 to Point/Station 702.000
**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 1082.000(Ft.)
Downstream point elevation = 983.000(Ft.)
Channel length thru subarea = 800.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 22.112(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 22.112(CFS)
Depth of flow = 0.457(Ft.), Average velocity = 16.615(Ft/s)
Channel flow top width = 3.827(Ft.)
Flow Velocity = 16.61(Ft/s)
Travel time = 0.80 min.
Time of concentration = 10.81 min.
Critical depth = 1.094(Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 3.356(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.829
Subarea runoff = 14.062(CFS) for 5.320(Ac.)
Total runoff = 29.095(CFS)
Effective area this stream = 10.46(Ac.)
Total Study Area (Main Stream No. 1) = 170.85(Ac.)
Area averaged Fm value = 0.265(In/Hr)
Depth of flow = 0.529(Ft.), Average velocity = 17.981(Ft/s)
Critical depth = 1.266(Ft.)

+++++
Process from Point/Station 701.000 to Point/Station 702.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 10.81 min.
Rainfall intensity = 3.356(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.834
Subarea runoff = 2.971(CFS) for 1.000(Ac.)
Total runoff = 32.066(CFS)
Effective area this stream = 11.46(Ac.)
Total Study Area (Main Stream No. 1) = 171.85(Ac.)
Area averaged Fm value = 0.247(In/Hr)

+++++
Process from Point/Station 701.000 to Point/Station 702.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 10.81 min.
Rainfall intensity = 3.356(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.830
Subarea runoff = 71.207(CFS) for 25.600(Ac.)
Total runoff = 103.273(CFS)
Effective area this stream = 37.06(Ac.)
Total Study Area (Main Stream No. 1) = 197.45(Ac.)
Area averaged Fm value = 0.259(In/Hr)

+++++
Process from Point/Station 702.000 to Point/Station 703.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

**** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 983.000(Ft.)
Downstream point elevation = 973.000(Ft.)
Channel length thru subarea = 435.000(Ft.)
Channel base width = 2.000(Ft.)
Slope or 'Z' of left channel bank = 2.000
Slope or 'Z' of right channel bank = 2.000
Estimated mean flow rate at midpoint of channel = 125.825(CFS)
Manning's 'N' = 0.015
Maximum depth of channel = 3.000(Ft.)
Flow(q) thru subarea = 125.825(CFS)
Depth of flow = 1.653(Ft.), Average velocity = 14.349(Ft/s)
Channel flow top width = 8.611(Ft.)
Flow Velocity = 14.35(Ft/s)
Travel time = 0.51 min.
Time of concentration = 11.32 min.
Critical depth = 2.563(Ft.)
Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 3.265(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.828
Subarea runoff = 45.032(CFS) for 17.800(Ac.)
Total runoff = 148.304(CFS)
Effective area this stream = 54.86(Ac.)
Total Study Area (Main Stream No. 1) = 215.25(Ac.)
Area averaged Fm value = 0.261(In/Hr)
Depth of flow = 1.782(Ft.), Average velocity = 14.964(Ft/s)
Critical depth = 2.750(Ft.)

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 973.000(Ft.)
Downstream point/station elevation = 953.000(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 148.304(CFS)
Nearest computed pipe diameter = 30.00(In.)
Calculated individual pipe flow = 148.304(CFS)
Normal flow depth in pipe = 24.33(In.)
Flow top width inside pipe = 23.49(In.)
Critical depth could not be calculated.
Pipe flow velocity = 34.78(Ft/s)
Travel time through pipe = 0.07 min.
Time of concentration (TC) = 11.39 min.

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 11.39 min.
Rainfall intensity = 3.253(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.828
Subarea runoff = 6.191(CFS) for 2.530(Ac.)
Total runoff = 154.496(CFS)
Effective area this stream = 57.39(Ac.)
Total Study Area (Main Stream No. 1) = 217.78(Ac.)
Area averaged Fm value = 0.261(In/Hr)

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 11.39 min.
Rainfall intensity = 3.253(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.829
Subarea runoff = 2.878(CFS) for 1.000(Ac.)
Total runoff = 157.374(CFS)
Effective area this stream = 58.39(Ac.)
Total Study Area (Main Stream No. 1) = 218.78(Ac.)
Area averaged Fm value = 0.258(In/Hr)

+++++
Process from Point/Station 703.000 to Point/Station 704.000
**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 1

Stream flow area = 58.390(Ac.)
Runoff from this stream = 157.374(CFS)
Time of concentration = 11.39 min.
Rainfall intensity = 3.253(In/Hr)
Area averaged loss rate (Fm) = 0.2579(In/Hr)
Area averaged Pervious ratio (Ap) = 0.9692

+++++
Process from Point/Station 705.000 to Point/Station 706.000
**** INITIAL AREA EVALUATION ****

COMMERCIAL subarea type

Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Initial subarea data:
Initial area flow distance = 800.000(Ft.)

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

Top (of initial area) elevation = 1058.800(Ft.)
 Bottom (of initial area) elevation = 1017.000(Ft.)
 Difference in elevation = 41.800(Ft.)
 Slope = 0.05225 s(%)= 5.22
 $TC = k(0.304)*[(length^3)/(elevation\ change)]^{0.2}$
 Initial area time of concentration = 7.952 min.
 Rainfall intensity = 4.034(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area (Q=KCIA) is C = 0.888
 Subarea runoff = 8.632(CFS)
 Total initial stream area = 2.410(Ac.)
 Pervious area fraction = 0.100
 Initial area Fm value = 0.055(In/Hr)

++++++
 Process from Point/Station 706.000 to Point/Station 707.000
 **** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****

Top of street segment elevation = 1017.000(Ft.)
 End of street segment elevation = 994.000(Ft.)
 Length of street segment = 485.000(Ft.)
 Height of curb above gutter flowline = 6.0(In.)
 Width of half street (curb to crown) = 16.500(Ft.)
 Distance from crown to crossfall grade break = 2.000(Ft.)
 Slope from gutter to grade break (v/hz) = 0.020
 Slope from grade break to crown (v/hz) = 0.020
 Street flow is on [1] side(s) of the street
 Distance from curb to property line = 13.500(Ft.)
 Slope from curb to property line (v/hz) = 0.025
 Gutter width = 2.000(Ft.)
 Gutter hike from flowline = 2.000(In.)
 Manning's N in gutter = 0.0150
 Manning's N from gutter to grade break = 0.0150
 Manning's N from grade break to crown = 0.0150
 Estimated mean flow rate at midpoint of street = 23.049(CFS)
 Depth of flow = 0.480(Ft.), Average velocity = 7.134(Ft/s)
 Note: depth of flow exceeds top of street crown.
 Streetflow hydraulics at midpoint of street travel:
 Halfstreet flow width = 16.500(Ft.)
 Flow velocity = 7.13(Ft/s)
 Travel time = 1.13 min. TC = 9.09 min.
 Adding area flow to street
 APARTMENT subarea type
 Decimal fraction soil group A = 0.000
 Decimal fraction soil group B = 0.000
 Decimal fraction soil group C = 1.000
 Decimal fraction soil group D = 0.000
 SCS curve number for soil(AMC 2) = 69.00
 Pervious ratio(Ap) = 0.2000 Max loss rate(Fm)= 0.110(In/Hr)
 Rainfall intensity = 3.724(In/Hr) for a 100.0 year storm
 Effective runoff coefficient used for area,(total area with modified
 rational method)(Q=KCIA) is C = 0.876
 Subarea runoff = 28.771(CFS) for 9.050(Ac.)
 Total runoff = 37.403(CFS)
 Effective area this stream = 11.46(Ac.)
 Total Study Area (Main Stream No. 1) = 230.24(Ac.)
 Area averaged Fm value = 0.098(In/Hr)
 Street flow at end of street = 37.403(CFS)
 Half street flow at end of street = 37.403(CFS)
 Depth of flow = 0.555(Ft.), Average velocity = 8.241(Ft/s)
 Warning: depth of flow exceeds top of curb
 Note: depth of flow exceeds top of street crown.
 Distance that curb overflow reaches into property = 2.21(Ft.)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

Flow width (from curb towards crown)= 16.500(Ft.)

+++++
Process from Point/Station 707.000 to Point/Station 708.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 987.000(Ft.)
Downstream point/station elevation = 967.000(Ft.)
Pipe length = 200.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 37.403(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 37.403(CFS)
Normal flow depth in pipe = 13.52(In.)
Flow top width inside pipe = 20.11(In.)
Critical depth could not be calculated.
Pipe flow velocity = 22.84(Ft/s)
Travel time through pipe = 0.15 min.
Time of concentration (TC) = 9.23 min.

+++++
Process from Point/Station 707.000 to Point/Station 708.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 9.23 min.
Rainfall intensity = 3.689(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area, (total area with modified
rational method) (Q=KCIA) is C = 0.874
Subarea runoff = 2.007(CFS) for 0.770(Ac.)
Total runoff = 39.410(CFS)
Effective area this stream = 12.23(Ac.)
Total Study Area (Main Stream No. 1) = 231.01(Ac.)
Area averaged Fm value = 0.109(In/Hr)

+++++
Process from Point/Station 708.000 to Point/Station 704.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 967.000(Ft.)
Downstream point/station elevation = 953.000(Ft.)
Pipe length = 150.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 39.410(CFS)
Nearest computed pipe diameter = 21.00(In.)
Calculated individual pipe flow = 39.410(CFS)
Normal flow depth in pipe = 14.39(In.)
Flow top width inside pipe = 19.51(In.)
Critical depth could not be calculated.
Pipe flow velocity = 22.43(Ft/s)
Travel time through pipe = 0.11 min.
Time of concentration (TC) = 9.34 min.

+++++
Process from Point/Station 708.000 to Point/Station 704.000

Roquet Ranch (TTM 19983) – Drainage Report

ATTACHMENT B

**** CONFLUENCE OF MINOR STREAMS ****

Along Main Stream number: 1 in normal stream number 2
 Stream flow area = 12.230 (Ac.)
 Runoff from this stream = 39.410 (CFS)
 Time of concentration = 9.34 min.
 Rainfall intensity = 3.663 (In/Hr)
 Area averaged loss rate (Fm) = 0.1086 (In/Hr)
 Area averaged Pervious ratio (Ap) = 0.2307
 Summary of stream data:

Stream No.	Flow rate (CFS)	Area (Ac.)	TC (min)	Fm (In/Hr)	Rainfall Intensity (In/Hr)
1	157.37	58.390	11.39	0.258	3.253
2	39.41	12.230	9.34	0.109	3.663
Qmax(1) =					
	1.000 *	1.000 *	157.374) +		
	0.885 *	1.000 *	39.410) + =		192.237
Qmax(2) =					
	1.137 *	0.820 *	157.374) +		
	1.000 *	1.000 *	39.410) + =		186.210

Total of 2 streams to confluence:
 Flow rates before confluence point:
 157.374 39.410
 Maximum flow rates at confluence using above data:
 192.237 186.210
 Area of streams before confluence:
 58.390 12.230
 Effective area values after confluence:
 70.620 60.138
 Results of confluence:
 Total flow rate = 192.237 (CFS)
 Time of concentration = 11.387 min.
 Effective stream area after confluence = 70.620 (Ac.)
 Study area average Pervious fraction (Ap) = 0.841
 Study area average soil loss rate (Fm) = 0.232 (In/Hr)
 Study area total (this main stream) = 70.62 (Ac.)

+++++
 Process from Point/Station 704.000 to Point/Station 709.000
 **** IMPROVED CHANNEL TRAVEL TIME ****

Upstream point elevation = 953.000 (Ft.)
 Downstream point elevation = 876.000 (Ft.)
 Channel length thru subarea = 1370.000 (Ft.)
 Channel base width = 5.000 (Ft.)
 Slope or 'Z' of left channel bank = 2.000
 Slope or 'Z' of right channel bank = 2.000
 Estimated mean flow rate at midpoint of channel = 210.578 (CFS)
 Manning's 'N' = 0.015
 Maximum depth of channel = 5.000 (Ft.)
 Flow (q) thru subarea = 210.578 (CFS)
 Depth of flow = 1.275 (Ft.), Average velocity = 21.882 (Ft/s)
 Channel flow top width = 10.099 (Ft.)
 Flow Velocity = 21.88 (Ft/s)
 Travel time = 1.04 min.
 Time of concentration = 12.43 min.
 Critical depth = 2.688 (Ft.)
 Adding area flow to channel

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Rainfall intensity = 3.086(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.830
Subarea runoff = 36.622(CFS) for 18.700(Ac.)
Total runoff = 228.859(CFS)
Effective area this stream = 89.32(Ac.)
Total Study Area (Main Stream No. 1) = 249.71(Ac.)
Area averaged Fm value = 0.239(In/Hr)
Depth of flow = 1.332(Ft.), Average velocity = 22.408(Ft/s)
Critical depth = 2.813(Ft.)

++++
Process from Point/Station 704.000 to Point/Station 709.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 12.43 min.
Rainfall intensity = 3.086(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.830
Subarea runoff = 22.341(CFS) for 8.800(Ac.)
Total runoff = 251.200(CFS)
Effective area this stream = 98.12(Ac.)
Total Study Area (Main Stream No. 1) = 258.51(Ac.)
Area averaged Fm value = 0.241(In/Hr)

++++
Process from Point/Station 704.000 to Point/Station 709.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 12.43 min.
Rainfall intensity = 3.086(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.831
Subarea runoff = 5.456(CFS) for 2.000(Ac.)
Total runoff = 256.656(CFS)
Effective area this stream = 100.12(Ac.)
Total Study Area (Main Stream No. 1) = 260.51(Ac.)
Area averaged Fm value = 0.238(In/Hr)

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

+++++
Process from Point/Station 800.000 to Point/Station 801.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Initial subarea data:
Initial area flow distance = 575.000(Ft.)
Top (of initial area) elevation = 1078.000(Ft.)
Bottom (of initial area) elevation = 986.000(Ft.)
Difference in elevation = 92.000(Ft.)
Slope = 0.16000 s(%)= 16.00
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.621 min.
Rainfall intensity = 3.599(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.834
Subarea runoff = 15.811(CFS)
Total initial stream area = 5.270(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.265(In/Hr)

+++++
Process from Point/Station 900.000 to Point/Station 901.000
**** INITIAL AREA EVALUATION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Initial subarea data:
Initial area flow distance = 573.000(Ft.)
Top (of initial area) elevation = 1095.000(Ft.)
Bottom (of initial area) elevation = 946.000(Ft.)
Difference in elevation = 149.000(Ft.)
Slope = 0.26003 s(%)= 26.00
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.718 min.
Rainfall intensity = 3.818(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.838
Subarea runoff = 13.110(CFS)
Total initial stream area = 4.100(Ac.)
Pervious area fraction = 1.000
Initial area Fm value = 0.265(In/Hr)

+++++
Process from Point/Station 900.000 to Point/Station 901.000
**** SUBAREA FLOW ADDITION ****

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000

Roquet Ranch (TTM 19983) – Drainage Report
ATTACHMENT B

SCS curve number for soil(AMC 2) = 86.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.265(In/Hr)
Time of concentration = 8.72 min.
Rainfall intensity = 3.818(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.838
Subarea runoff = 18.705(CFS) for 5.850(Ac.)
Total runoff = 31.815(CFS)
Effective area this stream = 9.95(Ac.)
Total Study Area (Main Stream No. 1) = 275.73(Ac.)
Area averaged Fm value = 0.265(In/Hr)

+++++
Process from Point/Station 902.000 to Point/Station 903.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****

Upstream point/station elevation = 940.000(Ft.)
Downstream point/station elevation = 936.000(Ft.)
Pipe length = 335.00(Ft.) Manning's N = 0.013
No. of pipes = 1 Required pipe flow = 31.815(CFS)
Nearest computed pipe diameter = 27.00(In.)
Calculated individual pipe flow = 31.815(CFS)
Normal flow depth in pipe = 20.81(In.)
Flow top width inside pipe = 22.70(In.)
Critical Depth = 23.31(In.)
Pipe flow velocity = 9.68(Ft/s)
Travel time through pipe = 0.58 min.
Time of concentration (TC) = 9.29 min.

+++++
Process from Point/Station 902.000 to Point/Station 903.000
**** SUBAREA FLOW ADDITION ****

COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 69.00
Pervious ratio(Ap) = 0.1000 Max loss rate(Fm)= 0.055(In/Hr)
Time of concentration = 9.29 min.
Rainfall intensity = 3.674(In/Hr) for a 100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method) (Q=KCIA) is C = 0.864
Subarea runoff = 39.132(CFS) for 12.410(Ac.)
Total runoff = 70.947(CFS)
Effective area this stream = 22.36(Ac.)
Total Study Area (Main Stream No. 1) = 288.14(Ac.)
Area averaged Fm value = 0.148(In/Hr)
End of computations, Total Study Area = 288.14 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.652
Area averaged SCS curve number = 77.8